



Synergetic Control of Non-Isolated 3-Φ Voltage & Current DC-Link EV Chargers

Source www.presentermedia.com



Daifei Zhang and Johann W. Kolar Swiss Federal Institute of Technology (ETH) Zurich Power Electronic Systems Laboratory www.pes.ee.ethz.ch

July 17, 2023







Synergetic Control of Non-Isolated 3-Φ Voltage & Current DC-Link EV Chargers

Abstract — The presentation first identifies Modularization, Functional Integration, Decentralization, Hybridization, and Synergetic Association as key concepts (*«*X-Concepts*»*) for future performance improvements of power electronics converters. Next, latest research results of the Power Electronic Systems Laboratory of ETH Zurich in the area of bidirectional three-phase AC/DC converter systems with voltage or current DC-link, i.e., boost-buck or buck-boost functionality, are discussed. The realization of both systems is based on "Synergetic Control" of the PFC rectifier input stage and DC/DC converter output stage and considers 400V line-to-line input, a very wide output voltage range of 200V to 1000V, and 10kW of rated power. The described hardware demonstrators are featuring high efficiency and power density and accordingly could serve as standard building blocks of galvanically isolated EV chargers. Moreover, as documented with the results of comprehensive experimental analyses, both systems are ideally suited as future RCD-based *non-isolated* EV chargers. The talk concludes with remarks on the urgency of a transition from a Linear Economy to a Circular Economy, which also needs to be considered for future power electronics converter designs in order to ensure that the 2050 Net-Zero-CO₂ target is reached on a sustainable basis.







Outline



- ► Introduction
- Voltage DC-Link AC/DC Boost-Buck Converter
 Current DC-Link AC/DC Buck-Boost Converter
 Future RCD-Based Non-Isolated EV Charger
- **Conclusions**







S-Curve of Power Electronics

- « X-Technologies » / "Moon-Shot" Technologies
 « X-Concepts » → Full Utilization of Basic Scaling Laws & X-Technologies
 Power Electronics 1.0 → Power Electronics 4.0









« X-Concepts »

Modularization Functional Integration Decentralization Hybridization Synergetic Association















Scaling of Multi-Cell/Level Concepts

- Reduced Ripple @ Same (!) Switching Losses Lower Overall On-Resistance @ Given Blocking Voltage Application of LV Technology to HV







• Scalability / Manufacturability / Standardization / Redundancy







15

20

99.35%

2.6kW/kg

56 W/in³

3-Φ Hybrid Multi-Level Inverter

- Realization of a 99%++ Efficient 10kW 3-Ф 400V_{rms,ll} Inverter System
 7-Level Hybrid Active NPC Topology / LV Si-Technology



• 200V Si \rightarrow 200V GaN Technology Results in 99.5% Efficiency















Isolated Matrix-Type 3-ΦPFC Rectifier (1)

- Based on Dual Active Bridge (DAB) Concept Ingegration of $3-\Phi$ PFC Rectifier & DC/DC Converter Stage Opt. Modulation ($t_1...t_4$) for Min. Transformer RMS Curr. & ZVS or ZCS Allows Buck-Boost Operation



• Equivalent Circuit

• Transformer Voltages / Currents







UtahStateUniversity

Isolated Matrix-Type 3-ΦPFC Rectifier (2)

















IIoT Starts with Sensors (!)

- **Condition Monitoring of DC Link Capacitors** On-Line Measurement of the ESR in *"Frequency Window"* (Temp. Compensated) Data Transfer by Optical Fibre or Near-Field RF Link





Source: Prof. Ertl TU Vienna, 2011

(hilinitute)

MICRO- 🕀

ΠŤ

CONTROLLER

ELECTROLYTIC CAPACITOR

DC LINK

BUS BARS

PCB

MONITORING BUS

 ${=}$





Additionally features Series Connect. Voltage Balancing















- Hybrid Combination of Mains- and Forced-Commutated Converter 3rd Harmonic Current Injection into Phase with Lowest Voltage Phase Selector AC Switches Operated @ Mains Frequency 3-Φ Unfolder



• Non-Sinusoidal Mains Current





15/54



IAF PFC Rectifier & Buck Converter Demonstrator







ETH zürich

Power Electronic Systems Laboratory













3-Φ EV-Charger Topology

- Isolated Controlled Output Voltage
 Buck-Boost Functionality & Sinusoidal Input Current
 Applicability of 600V GaN Semiconductor Technology
 High Power Density / Low Costs



 \rightarrow Conventional / Independent OR "Synergetic Control" of Input & Output Stage







Conventional Control — 3/3-PWM

- **Decoupled Control of AC/DC & DC/DC-Stage** Constant DC-Link Voltage (Equally Splitted) Cont. Sw. of All 3 Phases \rightarrow 3/3 PWM

 $D_{\bar{a}x}$

D.



→ Control Capability & Control DOFs NOT Fully Utilized (!)

╠╢┠╬

 $i_{\rm x}$ x

≑

+

 \mathbf{Z}

 $u'_{\rm xy} \prod P_{\rm xy}$

 $u'_{yz} \bigvee P_{yz}$





"Synergetic" Control — 1/3-PWM

- Only Phase with Lowest Current Switched Control of 2 Phase Currents by DC/DC-Stage Conduction Losses of the Switches \approx -80%
- Switching Losses $\approx -70\%$

 $D_{\bar{a}x}$

 D_{z}

600V GaN HEMTs Can be Used (!)



 \rightarrow Boost Capability Maintained (Transition from 1/3 to 3/3-PWM)

 $i_{\rm x}$ x

=

+

 \mathbf{Z}

āyā

 $u_{\mathbf{S}_{\bar{\mathbf{a}}\mathbf{y}\bar{\mathbf{a}}}}$







"Synergetic" Control — 3-Ф *Unfolder*

- **Mains-Frequency Commutated** NPCC Unfolder Cascaded by Dual-Bridge SRC DBSRC Regulates DC-Link Currents & Ultimately 3-\$\Phi\$ AC currents
- 93% @ 1.2 kW Bidirectional Power Flow



- Negligible Unfolder Switching Loss •
- Large DC-Link Voltage & Power Fluctuations









1/3-PWM — Analytical Derivation

• KVL of All Three Phases :

$$\begin{aligned} & -\frac{1}{2}U_{\rm DC} = u_{\rm yz} \le u_{\bar{\rm a}N} + u_{\rm CM} \le u_{\rm xy} = \frac{1}{2}U_{\rm DC} \\ & -\frac{1}{2}U_{\rm DC} = u_{\rm yz} \le u_{\bar{\rm b}N} + u_{\rm CM} \le u_{\rm xy} = \frac{1}{2}U_{\rm DC} \\ & -\frac{1}{2}U_{\rm DC} = u_{\rm yz} \le u_{\bar{\rm c}N} + u_{\rm CM} \le u_{\rm xy} = \frac{1}{2}U_{\rm DC} \end{aligned}$$

- CM Voltage Boundary :
 - $\begin{aligned} &-\frac{1}{2}U_{\text{DC}} u_{\min} \le u_{\text{CM}} \le \frac{1}{2}U_{\text{DC}} u_{\max} \\ &u_{\min} = \min(u_{\overline{a}N}, u_{\overline{b}N}, u_{\overline{c}N}) \\ &u_{\max} = \max(u_{\overline{a}N}, u_{\overline{b}N}, u_{\overline{c}N}) \end{aligned}$
- 1/3-PWM when Satisfying Two Equalities :

$$u_{\text{CM}} = -\frac{1}{2}(u_{\text{max}} + u_{\text{min}})$$









Typical EV Charger Structures

- Sustained Transportation Electrification
- More Compact & Efficient EV Chargers
- * Typical Structures of Isolated or Non-Isolated EV Charger





***** Typical Operating Range of 10kW Charger Module



• 3-Φ Non-Isolated Bidirectional AC/DC Converter System → Standard Building Block

• Buck-boost Capability : 200V to 1000V



23/54





3-Level DC/DC Buck Converter Stage

Simple & Non-Isolated Three-level Rare-End



 $3-\Phi$ Bb Voltage DC-Link PFC AC/DC Converter System •



- High Effective Sw. Frequency → Small Passive Components Volume
 Less Sw. Voltage → High Efficiency Operation
 Extended Output Voltage Range → 900V Devices for 1200V DC Output







— 3-Ф Bb Voltage DC-link PFC AC/DC Converter System —







Loss-Optimal Operating Principles

- **Buck**-Mode Operation 400V
- 1/3-PWM
- Pulse-Shape DC-Link Voltage



- Min. # of Switching Instants & Min. Amplitude of Switched Current
 App. 70% Reduction of Switching Losses





Loss-Optimal Operating Principles

- Transition-Mode Operation 540V
- Optimal 2/3-PWM[']
 Time-Varying DC-Link Voltage



- Seamless & Smooth Transition Between 1/3-PWM & 3/3-PWM
- Fully Utilize DC-Link Voltage Shape
 Avoid LF Current Flowing Through DC-Link Capacitors





28/54 ____



Loss-Optimal Operating Principles

- **Boost**-Mode Operation 800V
- 3/3-PWM
- Constant DC-Link Voltage



- Only Require Boost Functionality
 Permanently Turn DC/DC-Stage On → Avoid Sw. Losses







Synergetic Control Strategy





Output Voltage : $460V \rightarrow 600V \text{ w} / 50 \text{ Ohm Load}$ •





- Collaborative Operation of AC/DC & DC/DC Converter Stage
 Ensure Seamless / Democratic Transitions between Loss-Optimal Modes





Efficiency Measurement Results

Measurements Covering 200V to 800V & 25% Load to Full Load



• Peak Efficiency of 98.8%

• Up to 3.2% / 0.8% Efficiency Improvement in Buck-Mode / Transition-Mode Operations







VisitDUAITY(Boost-Buck-

Boost-Buck

Boost

ETH zürich



• "Boost-Buck" Translated into "Buck-Boost" Functionality / Lower # of Ind. Components





32/54



Bidirectional *Buck-Boost* **PFC** Rectifier Concepts

- Boost—Buck OR Buck—Boost Combination
- "Synergetic Control" of AC/DC and DC/DC Converter Stage



• AC/DC Buck-Stage Output Inductor Utilized as DC/DC Boost Inductor → Min. # of Inductive Components









3-Φ bB Current DC-link PFC AC/DC Converter System



200 ... 1000 V_{DC} | 10 kW @ 98.8% | 6.4 kW/L



ETH zürich

Loss-Optimal Operating Principles (1)



- Min. # of Switching Instants & Reduced Sw. Voltage \rightarrow App. 77% Reduction of Switching Losses
- Min. DC-Link Current \rightarrow 8% Reduction of Conduction Losses







Loss-Optimal Operating Principles (2)

- Buck-Mode Operation
- 3/3-PWM w/ Zero State
- Constant DC-Link Current

- Boost-Mode Operation
- 2/3-PWM w/o Zero State
- Pulse-shape DC-Link Current



- Min. # of Switching Instants & Reduced Sw. Voltage \rightarrow App. 77% Reduction of Switching Losses
- Min. DC-Link Current \rightarrow 8% Reduction of Conduction Losses







Synergetic Control Strategy

Enable 2/3-PWM with Variable DC-Link Current

Collaborative Operation of AC/DC & DC/DC Converter Stages



• Ensure Seamless / Democratic Transitions between Proposed Loss-Optimal Modes







Efficiency Measurement Results

Measurements Covering 200V to 1000V & 25% Load to Full Load







• Peak Efficiency of 98.8%

- Flat Efficiency Characteristic -- Above 98% in Most Area
- Up to 1% Efficiency Improvement in Boost-Mode Operation







Extended Synergetic Control









Two *Independently* Regulated DC Outputs





ETH zürich



— Experimental Comparison











Buck-Boost | **Boost-Buck** Demonstrator Systems

- **10 kW** @ 400...1000 V_{DC} @ 3-Φ 400 V_{rms} Mains
- $U_{out} = 200 \dots 1000 V_{DC}$ $\eta = 98.8\% @ 6.4 kW/dm^3$

- $\dot{AC}/DC f_{sw} = 100 \text{ kHz}$ $DC/DC f_{sw} = 2 \times 50 \text{ kHz}/100 \text{ kHz} eff.$

- 10 kW @ 400...800 V_{nc} @ 3-Φ 400 V_{rms} Mains
- $U_{out} = 200 \dots 800 V_{DC}$ $\eta = 98.8\% @ 5.4 \text{ kW/dm}^3$ $AC/DC f_{sw} = 100 \text{ kHz}$
- DC/DC $f_{sw}^{"}$ = 2x 100 kHz/200 kHz eff.





- *Min.* # of Inductive Components \rightarrow AC/DC Buck-Stage Output Inductor Utilized as DC/DC Boost Inductor
- Reduced Hardware Manufacture Cost & Complexity
- Reduced Control/Firmware Implementation Efforts







Demonstrator Systems *Measured Efficiency*

Buck-Boost Current DC-Link AC/DC Converter

Boost-Buck Voltage DC-Link AC/DC Converter



- Same # of Power Semiconductors & Similar Blocking Voltage Rating
 Current DC-Link : Dominant Cond. Losses → Flat Eff. Characteristic & High Partial-Load Eff.
- Voltage DC-Link : 3-L Front-End \rightarrow High Full-Load Eff.









Conducted EMI Pre-Compliance Tests

• Buck-Boost Current DC-Link AC/DC Converter

• **Boost-Buck** Voltage DC-Link AC/DC Converter



- Lower EMI Noise Emission Achieved by Advanced PWM Schemes
- Current DC-Link : Output Voltage Independent but Power Dependent
- Voltage DC-Link : DC-Link Voltage and Output Voltage Dependent
- **EMI Filter Redesign is Not Needed When Applying the Advanced PWM Schemes**







Future RCD-Based Non-Isolated EV Charger



Source: www.wolfspeed.com









3-Φ AC/DC Converter in EV Chargers

- **Galvanically Isolated EV Charger**
- Multi-Stage Structure
- 50 Hz Or HF Transformer (DAB, LLC, DCX...) Small Ground Current \rightarrow End-User Safety
- Bulky & Low Power Efficiency & High Cost



Non-Isolated EV charger

- Residual Current Device (RCD) \rightarrow End-User Safety Battery Package Parasitic Cap. up to Several uFs Min. Ground Current \rightarrow Avoid Nuisance Tripping

- Conv. EMI Filter Suppress HF Ground Current
- PV Inverter \rightarrow 1% More Efficiency w/ Half Volume Enable High Power On-Board Charger (OBC)









(ii) Proposed VGC

6(

(i) Conv.

Virtual Grounding Control (VGC)

Current DC-Link Rectifier Stage Generates LF CM Voltage
 Use DC/DC to Actively Compensate LF CM of AC/DC



- **Reduced LF CM** Noise Emission \rightarrow Time-Varying (150 Hz) Output Capacitor Voltage
- Similar DM Operations → Constant Output Voltage & 2/3-PWM







Experimental Verification

■ Output Midpoint Virtually Grounded to Input Capacitor Neutral & Mains PE ■ Increased Output Capacitance → High Cost & Low Power Density



Conventional Synergetic Control



• Closed-Loop Regulation of the Ground Current





Ground *Current* Control (GCC)

- Hard Connection between Output Midpoint & PE
- Direct Measure & Feedback Regulate Ground Current



• Ground Current: < 6 mA, Far Below 30 mA Limit

• Pre-Compliance Test Accord. to UL 2202 & IEC 61851 Considering TT & TN Systems







Conclusion & Summary

- Advanced PWM Schemes
- Current DC-Link: 2/3-PWM
- Voltage DC-Link: 1/3-PWM & 2/3-PWM-OPT
- Enables Optimal Clamping Operation
- **Synergetic Control Strategies**
- Loss-Optimal Buck-Boost Operation
 Seamless & Smooth Transitions Between Different Modes
- Independent Output Voltage/Power Control
- Fully Leverage Hardware Capacity
- Allow Loss-Opt. Operation for Voltage or Power Asymmetry
- Ground Current Control Strategy
- Target Future RCD-Based Non-Isolated EV Chargers
- Closed-Loop Regulation of Ground Current
 More Compact & Efficient EV Chargers



ETH zürich







Remark — All-Electric Society

- 25'000 GW of Installed Renewable Gen. & 15'000 GWh Batt. Storage
 4x Power Electronics Conversion Stages btw Generation → Load
 100'000 GW of Installed Converter Power
 20 Years of Useful Life

- $5'000 GW_{eq} = 5'000'000'000 kW_{eq}$ of Electronic Waste / Year (!)



UtahStateUniversity





The Paradigm Shift

- *"Linear" Economy / Take-Make-Dispose* \rightarrow *"Circular" Economy / Perpetual Flow of Resources Resources Returned into the Product Cycle at the End of Use*



Geographically Concentrated Production of Many Energy Transition Critical Minerals









Power Electronics 5.0









Further Reading

- D. Zhang, C. Leontaris, J. Huber, and J. W. Kolar, "Optimal Synergetic Control of High-Efficiency Three-Phase/Level Boost-Buck Voltage DC-Link Very Wide Output Voltage Range EV Charger," IEEE J. Emerg. Sel. Topics Power Electron. (Under Review). TechRxiv Preprint. DOI: https://doi.org/10.36227/techrxiv.22227889.v1
- D. Zhang, D. Cao, J. Huber, J. Everts, J. W. Kolar, "Non-Isolated Three-Phase Current DC-Link Buck-Boost EV Charger with Virtual Output Midpoint Grounding and Ground Current Control," IEEE Trans. Transp. Electrific. (Early Access). DOI: https://doi.org/10.1109/TTE.2023.3282978
- D. Zhang, D. Cao, J. Huber, and J. W. Kolar, "Three-Phase Synergetically Controlled Current DC-Link AC/DC Buck-Boost Converter with Two Independently Regulated DC Outputs," IEEE Trans. Power Electron., Vol. 38, No. 4, pp. 4195-4202, April 2023. DOI: https://doi.org/10.1109/TPEL.2022.3222236
- D. Zhang, M. Guacci, M. Haider, D. Bortis, J. W. Kolar, and J. Everts, "Three-Phase Bidirectional Buck-Boost Current DC-Link EV Battery Charger Featuring a Wide Output Voltage Range of 200 to 1000 V," Proc. IEEE Energy Conversion Congr. Expo. (ECCE USA), Detroit, MI, USA, 2020. DOI: https://doi.org/10.1109/ECCE44975.2020.9235868
- D. Zhang, M. Guacci, J. W. Kolar, and J. Everts, "Synergetic Control of a Three-Phase Buck-Boost Current DC-Link Bidirectional EV Battery Charger Considering Wide Output Range and Irregular Mains Conditions," Proc. IEEE Int. Power Electron. Motion Control Conf. (IPEMC-ECCE Asia), Nanjing, China, 2020. DOI: https://doi.org/10.1109/IPEMC-ECCEAsia48364.2020.9367853
- J. Azurza, M. Haider, D. Bortis, J. W. Kolar, M. Kasper, and G. Deboy, "New Synergetic Control of a 20kW Isolated VIENNA Rectifier Front-End EV Battery Charger," Proc. IEEE Workshop Control Modeling Power Electron. (COMPEL), Toronto, Canada, 2019. DOI: https://doi.org/10.1109/COMPEL.2019.8769657
- M. Guacci, D. Zhang, M. Tatic, D. Bortis, J. W. Kolar, Y. Kinoshita, and H. Ishida, "Three-Phase Two-Third-PWM Buck-Boost Current Source Inverter System Employing Dual-Gate Monolithic Bidirectional GaN e-FETs," CPSS Trans. Power Electron. Appl., Vol. 4, No. 4, pp. 339-354, December 2019. DOI: https://www.doi.org/10.24295/CPSSTPEA.2019.00032











