

A Gate Drive Circuit for Silicon Carbide JFET

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Abstract — In this paper, a gate drive circuit for a 1300V/4A SiC-JFET is proposed and evaluated experimentally for a switching frequency of 200kHz. Furthermore, a comparison of the switching behavior of a SiC-JFET/Si-MOSFET cascode and of the SiC-JFET driven by the proposed gate drive circuit is shown.

Index Terms — gate drive circuit; silicon carbide; JFET; switching behavior.

I. INTRODUCTION

Novel silicon carbide (SiC) power semiconductors are characterized by outstanding performance concerning voltage blocking capability, on-state voltage drop, switching speed, and thermal resistance [1]. Accordingly, future SiC devices will allow the realization of highly compact converter systems with low switching and conduction loss. Furthermore, due to the wide band gap and/or blocking capability SiC devices are suitable for high voltage applications. SiC Schottky-diodes are already available commercially [2] and the SiC turn-off power semiconductors are currently under development [3].

The characteristics of the gate current I_g versus the gate voltage V_g (with reference to source) of a SiC-JFET are shown in Fig.1. Since the SiC-JFET is normally-on device, a negative gate voltage is required for turning the device off. The pinch-off voltage is approximately $V_g = -30V$ [4]. However, considering the variation of the pinch-off voltage with junction

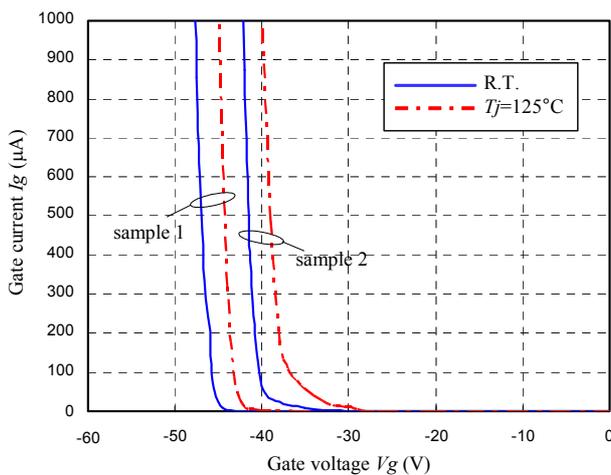


Fig.1: Gate characteristic of JFET samples at $T_j=25^\circ C$ and $T_j=125^\circ C$.

temperature and the influence of highly dynamic changes of the drain-source voltage on V_g via the Miller capacitance, a larger negative voltage should be applied for guaranteeing the power transistor turn-off state. This is complicated by the fact that the breakdown limit of the gate-source junction is around $-40V$ and/or close to the pinch-off voltage and varies between samples and shows a dependency on the junction temperature.

A SiC-JFET/Si-MOSFET cascode (hereafter called *cascode*) shown in Fig.2 can be turned off by using a silicon MOSFET (Si-MOSFET) connected in series with SiC-JFET [3]. However, there are several limitations of this concept as

- 1) the maximum operating temperature of the cascode is limited by the Si-MOSFET,
- 2) the Si-MOSFET internal diode shows a low dv/dt -rating and therefore does limit the admissible switching speed for applications in bridge-type circuit configurations, and
- 3) the conduction losses do increase as two devices are connected in series.

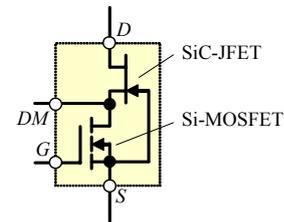


Fig.2: SiC-JFET / Si-MOSFET cascode.

Therefore, in this paper a gate drive circuit is proposed which does allow to safely operate a SiC-JET without employing a Si-MOSFET. The principle of operation of the gate drive is described in section II and experimentally verified in section III where also a comparison of the switching behavior of the SiC-JFET against the cascode arrangement is presented.

II. GATE DRIVE CIRCUIT FOR SiC-JFET

A simplified schematic of the proposed gate drive circuit is depicted in Fig.3. The SiC-JFET is turned on by turning on transistor $Tr1$ (cf. Fig.4) and turned off by $Tr2$ where an additional circuit is provided for limiting the gate current I_g as described in the following:

- $t1$: we have $V_g \approx 0V$ right after $Tr2$ is turned on, the resulting voltage V_r across the limiting circuit is shared by R_a and R_b and $Tr3$ is turned on. The gate current I_g is limited by R_g where

$R_g \ll Ra + Rb.$ (1)

The SiC-JFET is turned off when V_g exceeds the pinch-off

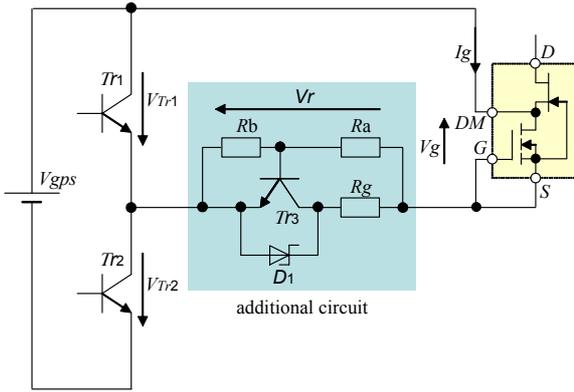


Fig.3: Simplified schematic of the proposed gate drive circuit for the SiC-JFET.

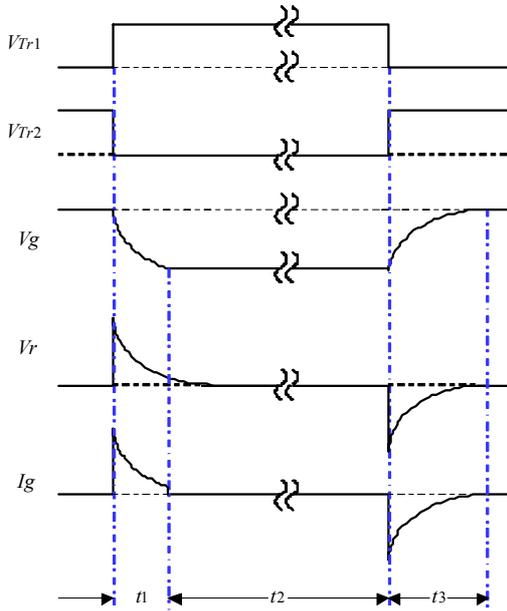


Fig.4: Operational principle of the proposed gate drive circuit.

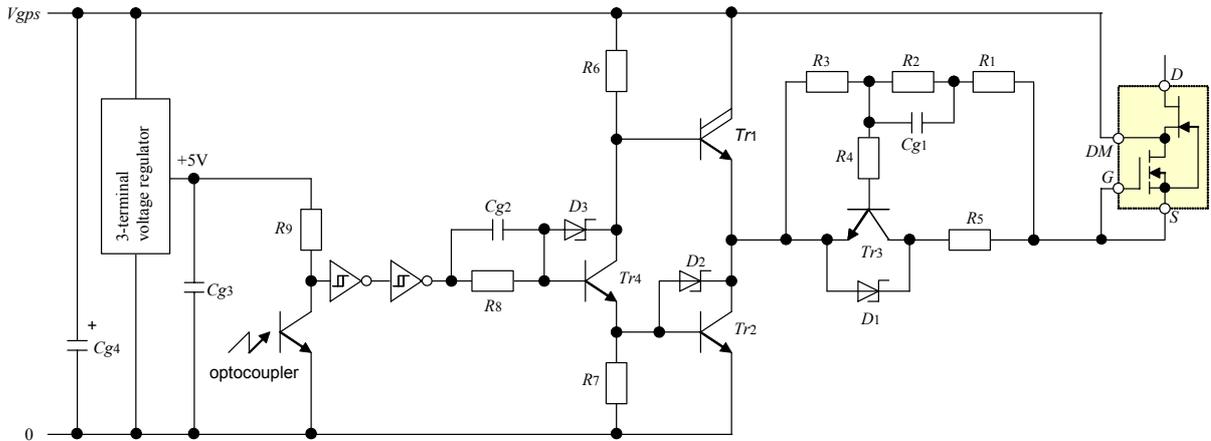


Fig.5: Schematic of the proposed gate drive circuit.

voltage. Subsequently, $Tr3$ is automatically turned off due to the decreasing voltage V_r .

t_2 : The transistor $Tr3$ is turned off and the current I_g is limited by the resistors R_a and R_b to a low value

$$I_g = \frac{V_{gps} - V_g - V_{Tr2}}{Ra + Rb} \quad (2)$$

where V_{gps} is supply voltage of the gate drive circuit and $V_{Tr2} \approx 0V$ is the voltage across $Tr2$.

t_3 : $Tr1$ is turned on and I_g is flowing through $Tr1$, $D1$ and R_g . As V_g reduces to zero the SiC-JFET is turned on.

In summary, the proposed gate drive circuit does prevent a high gate current in the turn-off interval also for applying a gate voltage higher than the pinch-off voltage and does ensure a high switching speed.

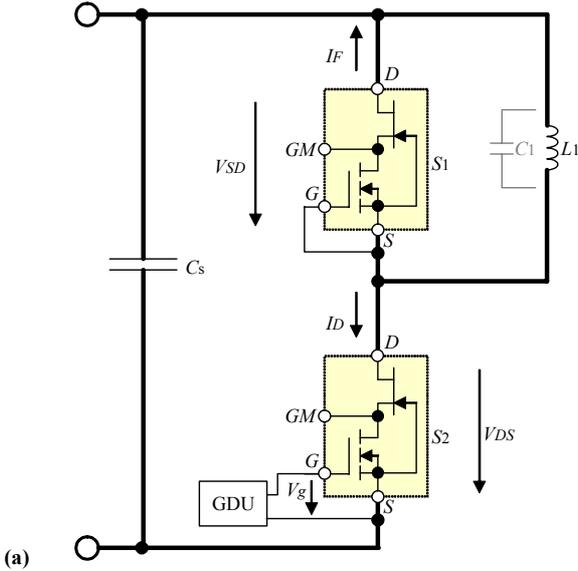
III. EXPERIMENTAL RESULTS

A. Experimental Condition

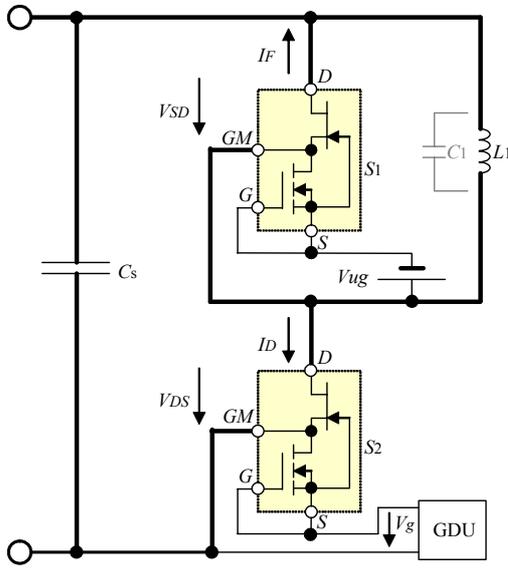
The gate drive circuit being employed for the experimental analysis is illustrated in **Fig.5**. In order to increase the turn-off speed of the SiC-JFETs, R_a (cf. Fig.3) is divided to R_1 and R_2 , and a capacitor C_{g1} is connected in parallel with R_2 . Furthermore, a resistor R_4 is provided for limiting the reverse current of the base-emitter junction of $Tr3$. In period t_1 (cf. Fig. 4), the base current in $Tr3$ is flowing largely via C_{g1} as R_2 shows a comparably high impedance what does result in a fast switching action of $Tr3$ and/or in a fast turn-off of the SiC-JFET. The DC supply voltage for the gate drive circuit is $V_{gps}=45V$ and V_{gps} is converted to 5V for supplying the driving optocoupler providing isolation of the gate drive signal. The Schottky diodes D_3 and D_2 are employed for increasing the turn-off speed in $Tr4$ and $Tr2$. The components employed in the gate drive circuit are listed in **TABLE I**. As the gate resistor, four $20\Omega/250mW$ resistors are connected in parallel ($R_5=5\Omega$ in total) because the design is for a switching frequency of 200kHz. Based on (2), $I_g < 370\mu A$ is guaranteed for a breakdown voltage of $V_g < 35V$.

TABLE I
COMPONENTS IN THE ADDITIONAL CIRCUIT

items	Symbols	Parameters / footprints
transistor	Tr_3	BC639, 80V, 1A / TO-92
diode	D_1	1N5711, 70V, 250mW
resistor	R_1	200 Ω , 250mW / 1206
	R_2	27k Ω , 250mW / 1206
	R_3	100 Ω , 250mW / 1206
	R_4	30 Ω , 250mW / 1206
	R_5	20 Ω , 250mW, 4 parallel / 1206
capacitor	C_{g1}	220pF / 1206



(a)



(b)

Fig.6: Circuit configurations for the testing of the cascodes (cf. (a)) and the SiC-JFETs (cf. (b)).

The circuit configurations for testing cascades and the corresponding SiC-JFETs are shown in **Fig.6**. The input voltage of the bridge leg is defined by a low inductance film capacitor C_s (9 μ F/630V), the load current is impressed by an inductor L_1 . The transistors S_1 are remaining in the turn-off state and are performing a free-wheeling diode function. There, for testing the SiC-JFETs a negative gate voltage $V_{ug}=-37$ V is applied (cf. Fig.6(b)) and for testing the cascode the terminals G and S of S_1 are short circuited (cf. Fig.6(a)). A conventional gate drive circuit with output voltage levels 0V, +14V is employed for driving the Si-MOSFET.

Two subsequent turn-on pulses are generated by a control circuit (not shown in Fig.6). Within the first pulse, the load current increases via S_2 . After a given current level has been reached the turn-off behavior of S_2 is recorded and the load current is commuted to the body diode of S_1 . When S_2 is turned on again, the turn-on behavior of S_2 and the reverse recovery behavior of S_1 are acquired.

The SiC-JFETs and the cascodes are mounted on a heatsink equipped with a heating resistor, which allows to operate the setup at an elevated junction temperature of 125°C. The gate drive and the testing power circuit which are placed on the same PCB are shown in **Fig.7**. The instruments utilized for the measurements were a Tektronix TDS 544A (500MHz, 1GS/s) oscilloscope, voltage probes LeCroy PP005 (10:1, 500V, 10M Ω /11pF, 500MHz), and an 1:50 AC current transducer employing a R10/N30 toroidal ferrite core, a burden resistor of 5 Ω and an adaptation network to a 50 Ω coaxial cable. The switching energy losses were calculated by multiplying the measured voltages and currents and integrating the resulting power losses.

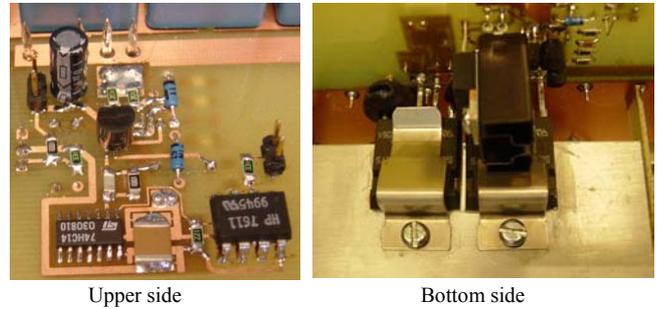


Fig.7: Prototype of the proposed gate drive circuit for the SiC-JFETs.

Reducing the parasitic capacitance of the load inductor is important for testing the actual switching performance and for reducing the switching losses [7]. Therefore, the load inductor L_1 (380 μ H/9A) is realized with low parasitic capacitance C_1 . There, four inductors each employing a ferrite core EPCOS B66291 with approximately 0.1mm air gap and 10 turns are connected in series and the individual turns are separated by selecting a wire of 1mm isolation thickness. According to the impedance measurement shown in **Fig.8**, C_1 is reduced to 2.7pF.

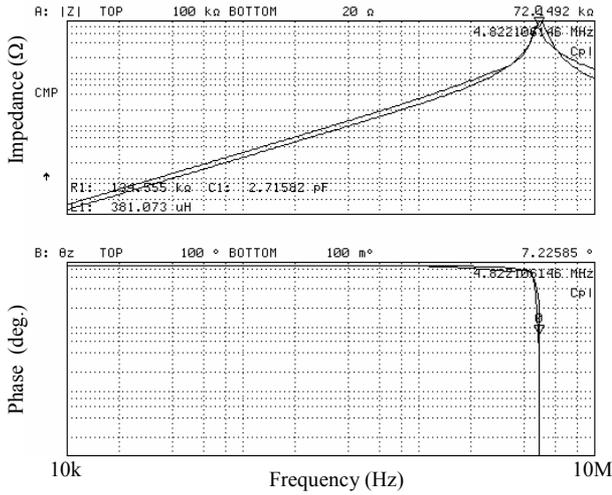


Fig.8: Frequency behavior of the impedance analysis of the load inductor L_1 .

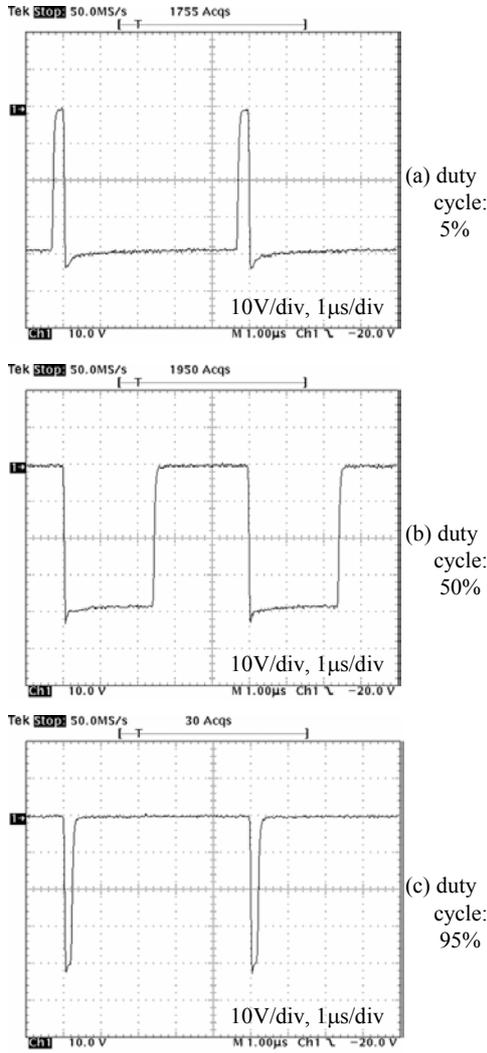


Fig.9: Gate voltage waveforms of the SiC-JFET (sample 2) driven by the proposed gate drive circuit at 200kHz , $T_j=125^\circ\text{C}$ and $I_D=0$.

B. Gate drive circuit

The operation of the proposed gate drive circuit was verified at zero drain current for a SiC-JFET showing a breakdown voltage of the gate-source junction lower than the gate drive supply voltage V_{gps} (sample 2, cf. Fig.1). The gate voltage waveforms V_g resulting for a switching frequency of 200kHz and a junction temperature of $T_j=125^\circ\text{C}$ are shown in Fig.9. In accordance to the theoretical considerations the maximum negative gate voltage is automatically limited to -38.5V where a gate current I_g of approximately $300\mu\text{A}$ does occur (cf. Fig. 1 and (2)). Then fall time and rise time of V_g are 40ns and 71ns respectively what does guarantee a high switching speed of the SiC-JFET.

C. Switching behavior

The results of a comparative analysis of the switching behavior of the cascode and the SiC-JFET in combination with

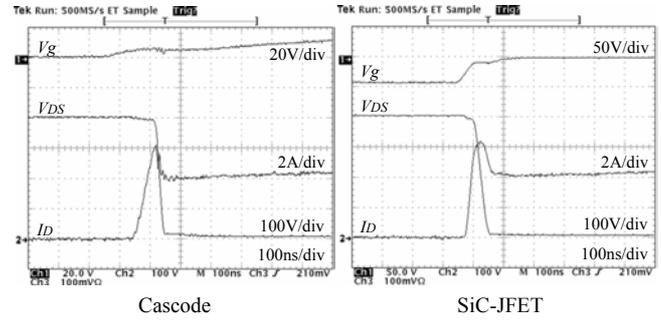


Fig.10: Turn-on behavior for $I_D=4\text{A}@T_j=125^\circ\text{C}$.

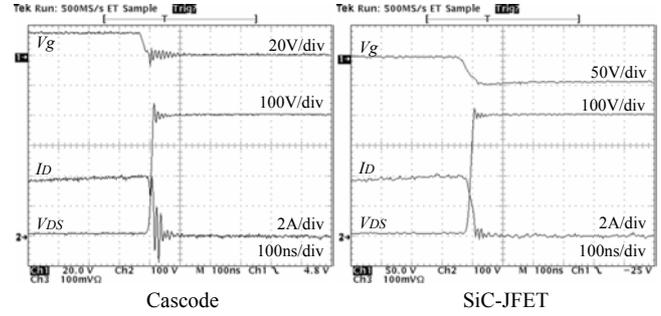


Fig.11: Turn-off behavior for $I_D=4\text{A}@T_j=125^\circ\text{C}$.

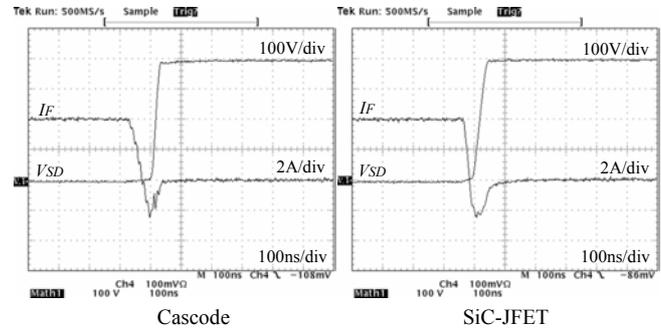


Fig.12: Reverse recovery behavior for $I_D=4\text{A}@T_j=125^\circ\text{C}$.

the proposed gate drive circuit are shown in **Fig.10**, **Fig.11** and **Fig.12** for $T_j=125^\circ\text{C}$. According to the specification of the body diode of the Si-MOSFET the dv/dt occurring across the transistor is limited to $6\text{kV}/\mu\text{s}$ by selecting a turn-on gate resistor of 390Ω and a turn-off gate resistor of 5Ω .

As compared to the cascode the SiC-JFET shows a reduced ringing at the switching transients [3]. Accordingly, no snubber circuit is required what does result in a compact converter design and low realization effort. The power semiconductor

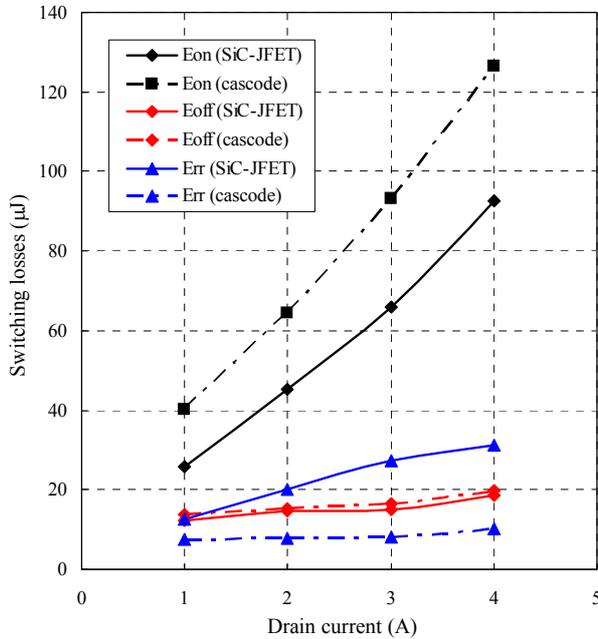


Fig.13: Switching losses versus drain current at $T_j=125^\circ\text{C}$.

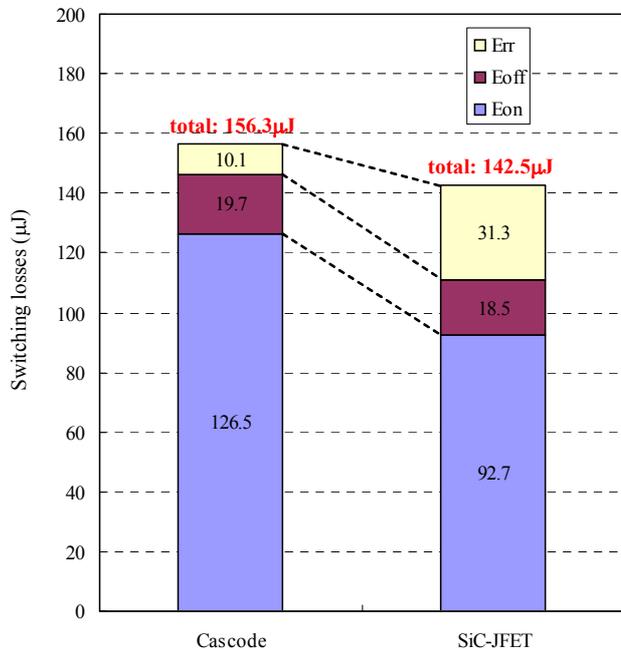


Fig.14: Comparison of the switching losses of the cascode and the SiC-JFET at $I_D=4\text{A}$ and $T_j=125^\circ\text{C}$.

switching losses are depicted in **Fig.13** and **Fig.14**. The reverse recovery losses Err of the cascode are lower than the corresponding losses of the SiC-JFET where a trade-off between Eon and $Eoff$ has to be considered. However, as compared to the cascode the SiC-JFETs shows lower turn-on and turn-off losses, i.e. the total switching losses are reduced from $156\mu\text{J}$ to $142\mu\text{J}$ (9%).

IV. CONCLUSION

A novel gate drive circuit for SiC-JFETs being able to operate at 200kHz switching frequency and ensuring high speed was proposed. As compared to a SiC-JFET/Si-MOSFET cascode the SiC-JFET in combination with the novel gate drive shows lower switching and conduction losses and reduced ringing at the switching transients.

In summary, a Si-MOSFET can be omitted for the realization of the SiC turn-off power semiconductor without impairing the switching performance. This does significantly reduce the realization effort and does make feasible an operation at elevated junction and/or heatsink temperatures and/or does enable the realization of converter systems showing high power density.

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