



GaN/SiC Monolithic Bidirectional Switches – Drivers of a Next Wave of Power Electronics Innovations

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... Let's Catch the Wave!

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GaN/SiC Monolithic Bidirectional Switches – Drivers of a Next Wave of Power Electronics Innovations



Abstract — Power Electronics is a key technology for all forms of generation and utilization of electric power in modern societies, ranging from renewable energy systems and highly diverse power supply applications including fast-charging of EVs and hyper-scale datacenters to variable frequency drives for industrial automation.

The progress in the area has been driven over the past 40 years by new power semiconductor device concepts and corresponding circuit topologies with a focus on voltage-source converter (VSC) structures and/or the application of switching elements limited to unipolar voltage-blocking capability. With reference to recently intensifying R&D activities on two-gate monolithic bi-directional switches (M-BDSs) featuring bipolar voltage blocking and bidirectional current control capability, the talk highlights the potential advantages of M-BDSs for the realization of ultra-compact non-isolated and isolated three-phase PFC rectifier systems and next generation inverter systems with low motor insulation stress. In this context, the performance gains achievable utilizing three-level T-type VSC topologies, new Solid-State-Transformer structures, and the unique features of current-source converter approaches – today solely employed in thyristor-based high-power medium-voltage motor drives – and AC/AC matrix converter concepts over state-of-the-art VSC systems are emphasized. Final considerations are on the paramount importance of minimization of life-cycle environmental impacts and/or ensuring circular economy compatibility of future power electronics systems for the next disruptive performance improvement towards Power Electronics 5.0.





Outline



- ► Introduction
- 3-Φ PFC Rectifiers
 3-Φ Variable Speed Motor Drives
 M-BDS R&D Activities
- ► Outlook



2023





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S-Curve of Power Electronics

- « X-Technologies » / "Moon-Shot" Technologies
 « X-Concepts » → Full Utilization of Basic Scaling Laws & X-Technologies
 Power Electronics 1.0 → Power Electronics 4.0
- 2...5...10x Improvement NOT Only 10% !







Global Megatrends



Renewable Energy Digitalization Sustainable Mobility Industry Automation Etc.







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Renewable Energy — **Photovoltaics**

- 3-Φ DC/AC Mains Interface
 Lower Costs / Higher Efficiency / Lower Weight
 20 Years Lifetime / Life-Cycle Assessment



Globally Installed PV Capacity Forecasted to 2.8 Terawatt by 2030 (IEA)







Digitalization — **Datacenters**

- Medium-Voltage \rightarrow Power-Supplies-on-Chip (0.6 ... 0.8V) Power Conversion
- Trend Towards 380V_{DC} Power Distribution
 Short Innovation Cycles
- Modularity / Scalability

Server-Farms up to **450 MW** 99.9999%/<30s/a \$1.0 Mio./Outage

> Since 2006 Running Costs > Initial Costs



- Higher Availability
- Higher Efficiency
 Higher Power Density
 Lower Costs



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3-Φ AC/DC Converter Application Areas

- Datacenter Power Supply
- Renewable Energy Applications
- **El.** Vehicle Battery Charging Full Rated Output for 3-Φ OR 1-Φ Grid





MPP Tracking in 60...90% of Max. Open Circuit Voltage

320...530V_{rms} Line-to-Line

- Non-Isolated OR Isolated Output
- Wide AC Input &/OR DC Output Voltage Range
- Unidirectional OR Bidirectional Power Transfer







3-Diode Bridge Rectifier

- *Conduction States Defined by Line-to-Line Mains Voltages Intervals with Zero Phase Current / LF Harmonics No Output Voltage Control*





→ Active Mains Current Shaping / Simultaneous Current Flow in All Phases





Integrated Active Filter (IAF) PFC Rectifier (1)

- **3rd Harmonic Current Injection** into Phase with Lowest Voltage Phase Selector AC Switches Operated @ Mains Frequency "3-Φ Unfolder" Input Stage







 \rightarrow DC/DC Output Stage — P₀= const. \rightarrow Sinusoidal Mains Current \rightarrow Uncontrolled Output Voltage





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Integrated Active Filter (IAF) PFC Rectifier (2)

- **3rd Harmonic Current Injection** into Phase with Lowest Voltage Phase Selector AC Switches Operated @ Mains Frequency "3-Φ Unfolder" Input Stage



• Non-Sinusoidal Mains Current



 \rightarrow DC/DC Output Stage — P₀= const. \rightarrow Sinusoidal Mains Current \rightarrow Controlled Output Voltage



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IAF Rectifier & Buck Output Stage





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 $u_{S\overline{S}}$

Drain/

Source

(S2)

 \overline{S}

 V_{G2S2}



• M-BDS \rightarrow Factor of 4 Reduction of Chip Area Comp. to Discrete Realization of Same $R_{(on)}$ (!)









- Realization of the Phase Selector Switches of 3rd Harmonic Inj. PFC Rectifiers
 Bipolar Voltage Blocking / Current Carrying Capability
 Low Sw. Frequ. / Mains Frequ. Operation



• M-BDS \rightarrow Factor of 4 Reduction of Chip Area Comp. to Discrete Realization of Same $R_{(on)}$ (!)





Swiss Rectifier

- **Integration** of 3rd Harmonic Injector Switches & Buck Output Stage Controlled Output Voltage Sinusoidal Mains Current

- i_y Def. by KCL: E.g. i_a i_c





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Swiss Rectifier Demonstrator

- **Efficiency** $\eta = 99.26\%$ @ 60% Rated Load Mains Current THD_I $\approx 0.5\%$ @ Rated Load Power Density $\rho \approx 4$ kW/dm³



- SiC Power MOSFETs & Diodes
- Integr. CM & Output Coupling Inductors (ICMCI)





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Remark M-BDS-Based 3rd Harm. Inj. Rectifiers

Bipolar Voltage Blocking / Current Carrying Capability

Factor of 4 Reduction of Chip Area Comp. to Discrete Realization of Same R_(on)



• Mains Frequ. Operation of the Phase Selector Switches \rightarrow Conduction Losses Only

















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3-Level T-Type PFC (Vienna) Rectifier

- **3**rd Harm. Inj. Inductor Shifted to AC-Side & PWM of DC-Midpoint Ref. Inj. Switches
- 3-Level Diode Bridge Input Voltage
- Sinusoidal Input Current
- Controlled Output Voltage



- Low Sw. Voltage Stress
- Low AC-Side Inductance
- Low Conduction Losses
- Bridge-Leg Symmetry & Phase Symmetry





Vienna Rectifier Demonstrator (1)

- Design for More Electric Aircraft Application
 650V CoolMOS & 1200V SiC Diodes
- Coldplate Cooling

 P_0 = 10 kW U_N = 400V_{AC}±10% f_N = 50Hz or 360...800Hz U_0 = 800V_{DC}



η =96.8%



• $THD_i = 1.6\% @ f_N = 800 \text{Hz} (f_P = 250 \text{kHz})$



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Vienna Rectifier Demonstrator (2)

- Design for More Electric Aircraft Application
 650V CoolMOS & 1200V SiC Diodes
- Coldplate Cooling

 P_0 = 10 kW U_N = 400V_{AC}±10% f_N = 50Hz or 360...800Hz U_0 = 800V_{DC}

η =96.8% $\dot{\rho} = 165 W/in^3 (10 kW/dm^3)$ $f_P = 250 kHz$



 l_{a}

- *THD_i* = 1.6% @ *f_N* = 800Hz
 System Allows 2-Φ Operation



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• *M-BDS-Realization of the Midpoint-Switches*

Significant Reduction of Cond. Losses @ Given Chip Area



• 600 V M-BDSs @ U_{pn}= 800 V_{DC} in Combination w/ 1200 V SiC Diodes (MOSFETs for Bidir. Power Flow)







Global Megatrends



Digitalization Renewable Energy Sustainable Mobility Industry Automation Etc.



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Electric Vehicle Outlook 2019

■ Bloomberg NEF — By 2040 — 57% of All Passenger Vehicle Sales 30% of Global Passenger Vehicle Fleet



Electric Cars Will Win on Price



Global long-term passenger vehicle sales by drivetrain

• Falling Battery Costs \rightarrow Price Parity of EVs & ICE-V by Mid-2020s \rightarrow Tipping Point for EV Industry







Disruptive Innovations

Example — Rapid Change of Transportation Enabled by New Technology (ICE) & Business Model Tony Seba: "All New Vehicles, Globally, will be Electric by 2030"

— NY City, 5th Av., Easter Parade → Year 1900: One Motor Cycle / Year 1913: One Horse & Carriage (!)



Source: Tony Seba

- Further Examples Digital / Analogue Photography, VHS Cassette Tape System / DVD etc.
- «The Stone Age Didn't End for the Lack of Stones» (Disrupted by Bronze Tools)







Ultra-Fast/High-Power EV Charging

- Modular Mains Interfaces | Future Non-Isolated Virtually Grounded Systems
 Very Wide Output Voltage Range (200...1000V)



ChargePoint stations (projected growth)

53,000 2019 2025 Source: ChargePoint



- Local Battery Buffer
- $320kW \rightarrow 400km$ Range in 20min







Bidir. *Boost-Buck* **PFC Rectifier Concepts**

- Vienna Rectifier Type Bidirectional Boost PFC AC/DC Front-End & DC/DC Buck Output Stage Coordinated "Synergetic Control" of AC/DC and DC/DC Converter Stage for Min. Sw. Losses



Future Non-Isolated EV-Charging \rightarrow Earth Leakage Curr. Limited Using "Virtual Ground Control"









Boost-Buck Buck-Boost



• "Boost-Buck" Translated into "Buck-Boost" Functionality / Lower # of Ind. Components







Bidir. Buck-Boost PFC Rectifier Concepts

- Boost—Buck OR Buck—Boost Combination
- Closed Loop vs. Open Loop Mains Current Control & Active Input Filter Damping
 "Synergetic Control" of AC/DC and DC/DC Converter Stage



AC/DC Buck-Stage Output Inductor Utilized as DC/DC Boost Inductor \rightarrow Min. # of Inductive Components





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Boost-Buck | Buck-Boost Demonstrator Systems

- 10 kW @ 400...800 V_{DC} @ $3-\Phi$ 400 V_{rms} Mains $U_{out} = 200 \dots 800 V_{DC}$ $\eta = 98.8\%$ @ 5.4 kW/dm³

- $AC/DC f_{sw} = 100 \text{ kHz}$ $DC/DC f_{sw} = 2 \times 100 \text{ kHz}/200 \text{ kHz} \text{ eff.}$

- **10 kW @ 400...1000 V**_{DC} @ $3-\Phi$ 400 V_{rms} Mains $U_{out} = 200 \dots 1000 V_{DC}$ $\eta = 98.6\%$ @ 6.4 kW/dm^3

- $AC/DC f_{sw} = 100 \text{ kHz}$ $DC/DC f_{sw} = 2 \times 50 \text{ kHz}/100 \text{ kHz} \text{ eff.}$



- **Boost-Buck** Voltage DC-Link PFC Rectifier
- **Buck-Boost** Current DC-Link PFC Rectifier







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- Boost—Buck OR Buck—Boost Combination
- Closed Loop vs. Open Loop Mains Current Control & Active Input Filter Damping
- "Synergetic Control" of AC/DC and DC/DC Converter Stage



• 600 V M-BDSs for Boost—Buck & 1200 V M-BDSs for Buck—Boost Combination @ 400 V_{rms} Mains

















Isolated Two-Stage 3-Φ AC/DC Converter

- 3- Φ AC/DC Converter Front-End Vienna Rectifier / Split DC-Link | f_{sw} =560 kHz 2x 2 Dual Active Bridge DC/DC Converter Isolation Stages | f_{sw} = 180...330 kHz



- 600V CoolGaN GIT HEMTs / 1200V CoolSiC Schottky Diodes
- Low Sw. Loss Synergetic Control of Input & Output Stage Six-Pulse-Shaped DC-Link Voltage





Isolated Single-Stage 3-Φ AC/DC Converter

- Low-Frequ. 3-Ø AC / High-Frequ. 1-Ø AC Matrix Converter Input Stage
 Converter Operation Based on the Dual Active Bridge (DAB) Concept
 Bidirectional Buck-Boost Operation

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• Equivalent Circuit

• Transformer Voltages / Currents



≈ 99%

 $\begin{array}{l} f_{\rm sw} = 31\,\rm kHz\\ f_{\rm sw} = 36\,\rm kHz\\ f_{\rm sw} = 41\,\rm kHz\\ f_{\rm sw} = 50\,\rm kHz\\ f_{\rm sw} = 60\,\rm kHz \end{array}$

22

10A/div

200V/div

18

Isolated Matrix-Type 3-PFC Rectifier Demonstrator



900V / 10m\Omega SiC Power MOSFETs Opt. Modulation Based on 3D Look-Up Table



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- Functional Integration \rightarrow Lower Complexity BUT Limited Controllability Rated 3- Φ Output Power NOT Available in 1- Φ Line-to-Line Operation
- Rated Power Operation for 3- ϕ AND 1- ϕ Grid Connection \rightarrow Requires Phase-Modular Input Stage







New 3-Φ OR 1-Φ Input ─── Full Rated Power Operable Single− ── Stage Isolated PFC Rectifier





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3-Φ Input DAB-Type AC/DC Converter

- Modification of 3- Φ Xfrm DAB \rightarrow Prim.-Side Phase-Modular AC/DC Converter Synchronized (!) Prim.-Side Switching @ 50% Duty Cycle
- DAB-Type OR Series Res. Converter Operation





- Voltage Stress on AC-Side Power Transistors Determined by PHASE Voltage Amplitude (!)
- 600V GaN MBDS for 400V RMS Line-to-Line Grid ($U_{pk} = 560V$)
- Unity Power Factor / Bidirectional





Remark 3-O Input Single-Stage Isol. PFC Rectifier

- Full Rated Power Operation @ 3-Φ AND 1-Φ Grid Input (!)
- Synchronized (!) Prim.-Side Switching @ 50% Duty Cycle | L_{stray}, C_{res} Tuned to f_{sw} Sec.-Side Replicates Prim.-Side Voltage Local Avg. Values @ 2 x f_{sw}

 $U_{\rm dc}$

 $\underline{\mathcal{U}}_{\text{Tabe}}$

+



Boost Operation w/ Sec.-Side Zero Volt. Intervals | Buck Operation w/ Prim.-Side Zero Volt. Intervals

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Sinusoidal Grid Currents / Bidirectional Power Flow

 L_{\circ}

(!)

 C_{\circ}

(m)

 $\underline{u}_{\text{TABC}}$

0

Time (ms)



Time (µs)

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Ν

⊶



 $N_1:N_2 = 1:1$

Remark 1-**D** Input Single-Stage Isol. PFC Rectifier

- All Prim.-Side Phase Modules Operated in Parallel
- 120° Phase-Shifted Sw. @ 50% Duty Cycle & Res. Frequency
- 3-Φ Sw. Frequ. Six-Step Voltage Syst. Applied to Xfrm Primary Sec.-Side Mod. Replicates Prim.-Side Phase Voltage Local Avg. Values



- **Boost Operation** w/ Sec.-Side Zero Volt. Intervals
- Buck Operation w/ Prim.-Side Zero Volt. Intervals

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Sinusoidal Grid Currents / Bidirectional Power Flow





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3-Φ & **1-Φ** Full Power Operable PFC Rectifier

- Voltage Stress on AC-Side Power Transistors Determined by PHASE Voltage Amplitude (!)
- 600V GaN MBDS for 400V RMS Line-to-Line Grid ($U_{L-L,pk} = 560V$) Unity Power Factor / Bidirectional





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Classification of Isolated PFC Rectifier Topologies



• Numerous New BDS-Based Single-Stage Conv. Concepts & Related Mod. Schemes (!)







Global Megatrends









Variable Speed Motor Drive (VSD) Systems

- Industry Automation / Robotics
 Material Machining / Processing Drilling, Milling, etc.
- Compressors / Pumps / Fans
- Transportation
- etc., etc.

.... Everywhere !



• 60...70 % of All Electric Energy Used in Industry Consumed by VSDs





Variable Speed Drive Concepts

- **DC-Link Based AC/DC/AC OR Matrix-Type AC/AC Converters Battery OR Fuel-Cell Supply OR Common DC-Bus Concepts**



• 45% of World's Electricity Used for Motors in Buildings & Industrial Applications







Current DC-Link *Buck-Boost* Inverter (1)

Derivation Based on Bidirectional Buck-Boost PFC Rectifier Topology (EV Charger) Lower # of Ind. Components Compared to Boost-Buck Approach



•

DC/DC Buck Converter Performs Voltage \rightarrow **Current Translation** Coordinated Control / Modulation of DC/DC & Inverter Stage for Min. Sw. Losses





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Current DC-Link *Buck-Boost* Inverter (2)

- *"Synergetic" Control of DC/DC Buck Converter & Current DC-Link Inverter Stage 6-Pulse-Shaping of DC Current by Buck-Stage* \rightarrow *Allows Inverter Phase Clamping*



Switching of Only 2 of 3 Phase Legs \rightarrow Reduction of Sw. Losses by \approx 86% (!)













3-Φ Current DC-Link AC/AC Converter (1)

DC-Side Coupling of Buck-Boost Current DC-Link PFC Rectifier & Inverter — AC/DC/AC

Full Sinewave Filtering @ Input & Output w/ Single Magnetic Component



• Bipolar Blocking / Unidir. Switches / Unidir. DC-Link Current Sufficient for Bidir. Power Conversion

• Modulation-Based Inversion of DC-Link Voltage Polarity \rightarrow Inv. of Power Flow Direction







3-Φ Current DC-Link AC/AC Converter (2)



• Relation to High-Power Thyristor-Based Medium Voltage Synchr. Machine Variable Speed Drives







Remark Self Reverse-Blocking M-BDS (1)

- **Bidir.** Curr. DC-Link Converters Unidir. I_{dc} & Bipolar U_{dc} OR **Bidir.** I_{dc} & Unipolar U_{dc}
- HV Switch + HV Diode
 M-BDS

• "Self-Switching"

HV Diode Characteristic / High Cond. Losses Ohmic Cond. Char. BUT 2 External Gate Signals / 2 Gate Drives Ohmic Cond. Char. BUT High Local Complexity (Sensing)



SRB-MBDS Quasi-Ohmic Cond. Char. (Cascode w/ LV Si Schottky Diode) & 1 External Gate





Remark Self Reverse-Blocking M-BDS (2)

- **Bidir.** Curr. DC-Link Converters Unidir. I_{dc} & Bipolar U_{dc} OR **Bidir.** I_{dc} & Unipolar U_{dc}
- HV Switch + HV Diode
 M-BDS

• "Self-Switching"

HV Diode Characteristic / High Cond. Losses Ohmic Cond. Char. BUT 2 External Gate Signals / 2 Gate Drives Ohmic Cond. Char. BUT High Local Complexity (Sensing)



SRB-MBDS Quasi-Ohmic Cond. Char. (Cascode w/ LV Si Schottky Diode) & 1 External Gate







- Current DC-Link Topology
- Application of (SRB)-M-BDSs Complex 4-Step Commutation OR SRB-M-BDSs
- Moderate Filter Volume



- Challenging Overvoltage Protection
- Limited Control Dynamics

- Voltage DC-Link Topology
- **Standard** Bridge-Legs
- Low-Complexity Commutation Defined Semiconductor Voltage Stress
- Facilitates DC-Link Energy Storage



High Input / Output Filter Volume







DUA

- Current DC-Link Topology
- Application of (SRB)-M-BDSs Complex 4-Step Commutation OR SRB-M-BDSs Moderate Filter Volume

- Voltage DC-Link Topology
- **Standard** Bridge-Legs
- Low-Complexity Commutation Defined Semiconductor Voltage Stress
- Facilitates DC-Link Energy Storage





■ All-600V-GaN AC-AC VSDs / 1.4 kW, 200 V L-L / Full EMI Filter (Grid & Motor) / 97% Nominal Eff.









$3-\Phi AC/AC$ Matrix Converter $\begin{cases} 1 0 0 \\ 0 0 0 \\ 0 1 1 \end{cases}$



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Indirect & *Direct* 3-Φ AC/AC Matrix Converter (1)

- Constant 3- \oplus Instantaneous Power Flow \rightarrow No Low-Frequ. DC-Link Power Pulsation Buffer Requirement (!)
- Indirect AC/DC—DC/AC OR Direct AC/AC Power Conversion \rightarrow IMC OR DMC Switch Matrix w/ Bipolar Voltage Blocking & Current Carrying Devices



Output-Side Motor Inductor \rightarrow Operation Limited to Buck-Type (Step-Down) Voltage Conversion





Indirect & *Direct* 3-Φ AC/AC Matrix Converter (2)

Input Filter Capacitors | Sw. Stage | Motor Inductance
 Buck-Type Power Conversion Topology





- IMC Relies on Strictly Pos. DC-Link Voltage / i=0 Input Stage Commutation
- M-BDS-Based Realization of DMC Features Lower # of Switches / 4-Step Commutation Required









- Indirect Matrix Converter (IMC)
- **M-BDS** AC/DC Front-End ZCS Commutation of AC/DC Stage @ i_{DC} =0 No 4-Step Commutation

- Direct Matrix Converter (DMC)
- 4-Step Commutation Exclusive Use of M-BDSs



- **Higher # of Switches Compared to DMC**
- Lower Cond. Losses @ Low Output Voltage Thermally Critical @ $f_{out} \rightarrow 0$



• Thermally Critical @ $f_{out} \approx f_{in}$















Four-Quadrant Cascode GaN Switch (FQS)

■ Common-Drain Arrangement of Two Cascode Switches (600V GaN D-Mode HEMT + LV Si E-Mode MOSFET)

Up to 1200V Samples for Demonstration Purposes



- 4Q Current Conduction Only in Quadrants I & III
- Shared Drift Region for Blocking Pos. & Neg. Voltage & Separate Cascode MOSFETs



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Exp. Analysis of 1st Gen. 600V GaN M-BDS

- PowerAmerica Program Based on Infineon's CoolGaN™ HEMT Technology Dual-Gate Device / Controllability of Currents in Both Directions
- Bipolar Voltage Blocking Capability | Normally-On or Normally-Off



- Analysis of 4-Quardant Operation of $R_{DS(on)}$ = 140m $\Omega \mid 600V$ Sample @ ± 400V Shared Drift Region \rightarrow "True" Monolithic Bidirectional Switch (TM-BDS)





Monolithic Bidirectional **Diamond Switch**

Diamond — High Breakdown Field / High Carrier Mobility / High Therm. Conductivity Lateral / Single Drift Layer Double-Gate Reverse Blocking & Reverse Conducting Power MOSFET



- Very Basic Proof of Concept @ 250°C
- Lateral Bidir. Diamond Devices Could Outperform Bidir. Vertical 4H-SiC Devices @ High Temp.



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Monolithically Integr. Bi-Directional 15kV SiC IGBT

- Planar-Gate Bi-Direct. IGBT Fabricated w/ Double-Sided Lithography Process on Free-Standing n[—] Wafers MOS-Cells on Both Sides of Lightly Doped Drift Region / Cond. & Sw. Loss Infl. by Back-Side Gate Volt. Bias
- Challenging Packaging & Cooling



- Simul. Performance of a 15kV BD-IGBT | Blocking Characteristic (max. 7.2 kV Meas.) Epi Layer Defects etc.
 Shared Drift Region → "True" Monolithic Bidirectional Switch (TM-BDS)



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Remark Solid-State Circuit Breakers (SSCBs)

- Ultra-Fast Fault Interruption | Reduced Fault Stress | Arc-Less | Low Surge Voltage | Long Lifetime
- Software / Remote Configurable Trip Behavior / Remote-Controlled Load Switch



Rodrigues et al., 2021

- Recent LV Example w/ Custom SiC Modules / Max. 100 A Cont. / UL Certified M-BDSs Low On-Resistance Mandatory (e.g. 1100V, 22m Ω GaN M-BDS) | Low Leakage Current

















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- 25'000 GW Installed Ren. Generation in 2050
- **15'000 GWh** Batt. Storage
- 4x Power Electr. Conversion btw Generation & Load
- 100'000 GW of Installed Converter Power
- **20 Years** of Useful Life



5'000 GW_{eq} = 5'000'000'000 kW_{eq} of E-Waste / Year (!)
 10'000'000'000 \$ of Potential Value



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The Paradigm Shift

- *"Linear" Economy / Take-Make-Dispose* \rightarrow *"Circular" Economy / Perpetual Flow of Resources Resources Returned into the Product Cycle at the End of Use*



Geographically Concentrated Production / Processing of Many Energy Transition Critical Minerals







Power Electronics 5.0









Thank You !





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