



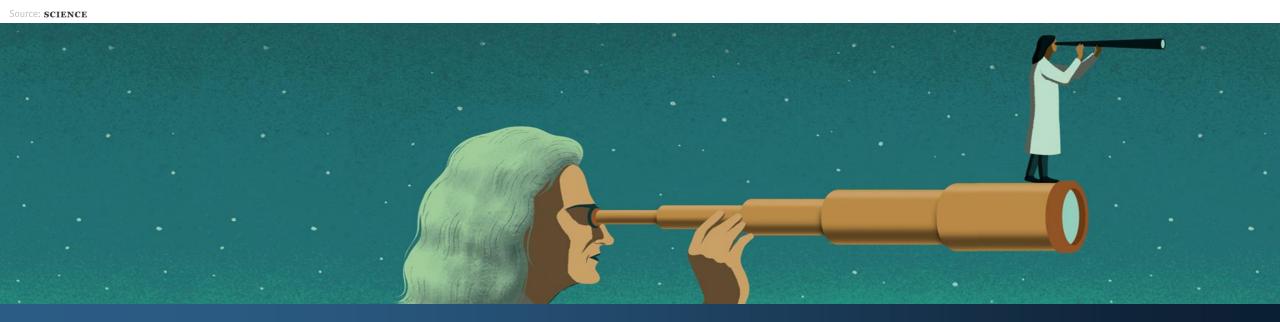
Power Electronics 5.0 Standing on the Shoulders of Giants

Johann W. Kolar et al.



Swiss Federal Institute of Technology (ETH) Zurich Power Electronic Systems Laboratory www.pes.ee.ethz.ch

Sept. 25, 2023







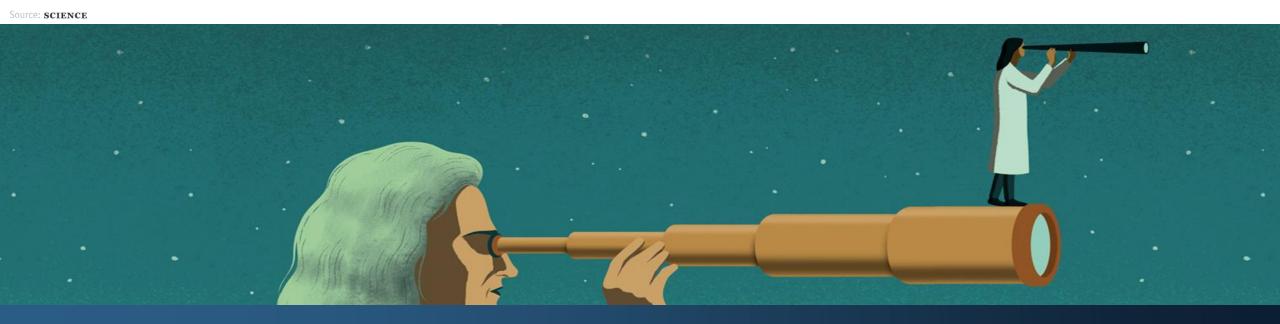
Power Electronics 5.0 Standing on the Shoulders of Giants

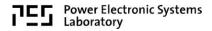
Johann W. Kolar | Jonas E. Huber | Daifei Zhang | David Menzi | Neha Nain



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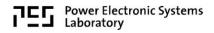
"Power Electronics 5.0"— Standing on the Shoulders of Giants

Abstract—Power electronics is a key technology for all forms of generation and utilization of electric power in modern societies, ranging from renewable energy systems and highly diverse power supply applications, including fast-charging of EVs and hyper-scale datacenters, to variable-frequency drives for industrial automation. Over the past 40 years, the progress in the area has been driven by new power semiconductor device concepts and corresponding circuit topologies with a focus on voltage-source converter (VSC) structures and/or the application of switching elements limited to unipolar voltage-blocking capability.

With reference to recently intensifying R&D activities on two-gate monolithic bidirectional switches (M-BDSs) featuring bipolar voltage blocking and bidirectional current control capability, the talk highlights the potential advantages of M-BDSs for the realization of ultra-compact non-isolated and isolated three-phase PFC rectifier systems and next-generation inverter systems with low motor insulation stress. In this context, the performance gains achievable with three-level T-type VSC topologies, new single-stage isolated AC/DC converter structures, and the unique features of current-source converter approaches—today solely employed in thyristor-based high-power medium-voltage motor drives—and AC/AC matrix converter concepts over state-of-the-art VSC systems are emphasized. All this identifies M-BDSs as one of the main drivers of a 4th wave of disruptive performance improvements of power electronic converter systems. The talk will conclude with remarks on the urgency of a transition from a linear economy to a circular economy, which also needs to be considered for future power electronic converter designs. Building on the understanding and knowledge gained by brilliant engineers over the last decades, i.e., standing on the shoulders of giants, power electronics research must now target "beyond tomorrow" improvements and enable a circular-economy-compatible Power Electronics 5.0 in order to ensure that the 2050 net-zero-CO₂ target is reached on a sustainable basis.









Outline



- **►** Introduction
- 3-Φ AC/DC Grid Interfaces
 3-Φ AC/AC VSD Converter Systems
 GaN/SiC M-BDS R&D Activities
- **▶** Outlook

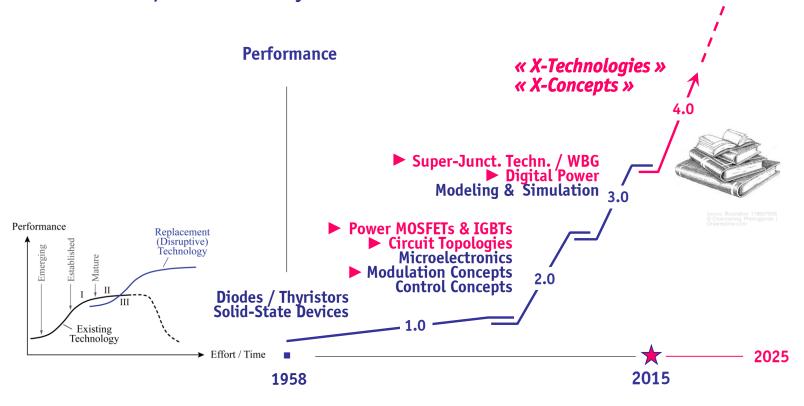






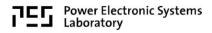
S-Curve of Power Electronics

- « X-Technologies » / "Moon-Shot" Technologies
 « X-Concepts » → Full Utilization of Basic Scaling Laws & X-Technologies
 Power Electronics 1.0 → Power Electronics 4.0
- 2...5...10x Improvement NOT Only 10%!











Global Megatrends



Renewable Energy
Digitalization
Sustainable Mobility
Industry Automation
Etc.

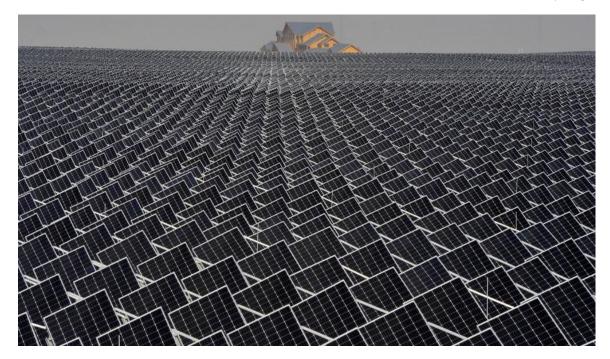




Renewable Energy – Photovoltaics

- 3-Φ DC/AC Mains Interface Lower Costs / Higher Efficiency / Lower Weight 20 Years Lifetime / Life-Cycle Assessment

Source: REUTERS/Stringer



■ Globally Installed PV **Capacity** Forecasted to 2.7 Terawatt by 2030 (IEA)





Digitalization — **Datacenters**

- Medium-Voltage → Power-Supplies-on-Chip (0.6 ... 0.8V) Power Conversion
 Trend Towards 380V DC Power Distribution
- Short Innovation Cycles
- *Modularity / Scalability*

Server-Farms up to **450 MW** 99.9999%/<30s/a \$1.0 Mio./Outage

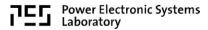
> Since 2006 Running Costs > Initial Costs



- Higher Availability
- Higher EfficiencyHigher Power Density
- Lower Costs



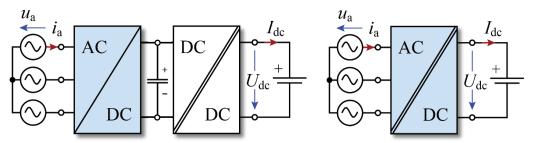


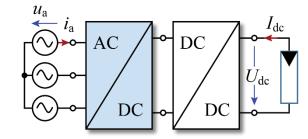


3-Ф AC/DC Converter Application Areas

- Datacenter Power Supply
- Electric Vehicle Battery Charging
- Renewable Energy Applications

Typ. 200...1000V_{DC} EV Battery Voltage Range





320...530V_{rms} Line-to-Line MPP Tracking in 60...90% of Max. Open Circuit Voltage

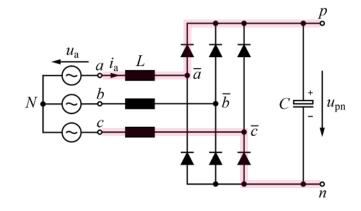
- Non-Isolated OR Isolated Output
- Wide AC Input &/OR DC Output Voltage Range
- Unidirectional OR Bidirectional Power Transfer

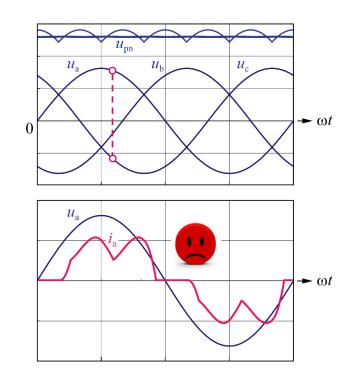




3- Diode Bridge Rectifier

- Conduction States Defined by Line-to-Line Mains Voltages
 Intervals with Zero Phase Current / LF Harmonics
 No Output Voltage Control





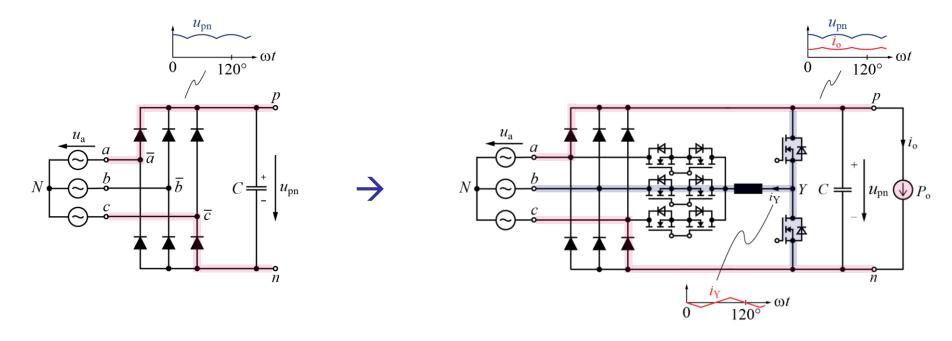
→ Active Mains Current Shaping / Simultaneous Current Flow in All Phases





Integrated Active Filter (IAF) PFC Rectifier

- 3rd Harmonic Current Injection into Phase with Lowest Voltage
 Phase Selector AC Switches Operated @ Mains Frequency "3-Φ Unfolder" Input Stage



Non-Sinusoidal Mains Current

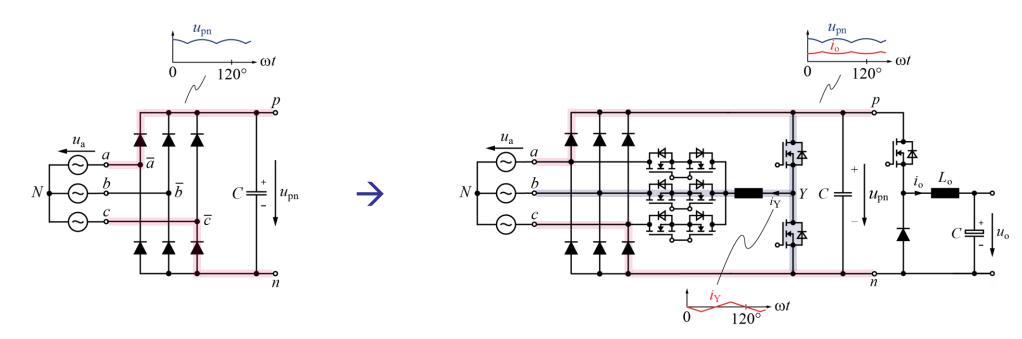
- \rightarrow DC/DC Output Stage P_0 = const. \rightarrow Sinusoidal Mains Current
- → Controlled Output Voltage





Integrated Active Filter (IAF) PFC Rectifier

- 3rd Harmonic Current Injection into Phase with Lowest Voltage Phase Selector AC Switches Operated @ Mains Frequency "3-Ф Unfolder" Input Stage



Non-Sinusoidal Mains Current

- \rightarrow DC/DC Output Stage P_0 = const. \rightarrow Sinusoidal Mains Current
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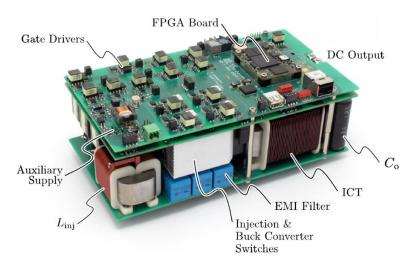




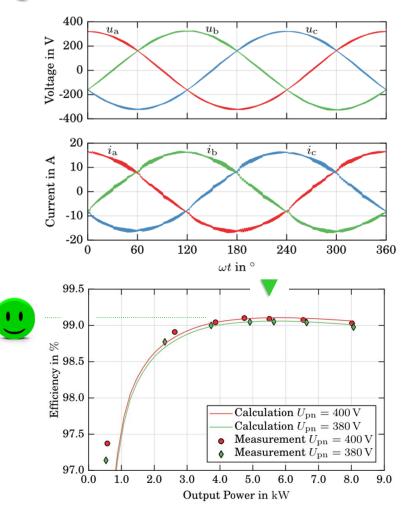
IAF Rectifier & Buck Output Stage

- Efficiency $\eta > 99.1\%$ @ 60% Rated Load Mains Current THD_I $\approx 2\%$ @ Rated Load Power Density $\rho \approx 4 \text{kW/dm}^3$

$$P_0$$
= 8 kW
 U_N = 400V_{AC} $\rightarrow U_0$ = 400V_{DC} const. / Controlled
 f_S = 27kHz



- SiC Power MOSFETs & Diodes
- 2 Interleaved Buck DC/DC Output Stages (!)



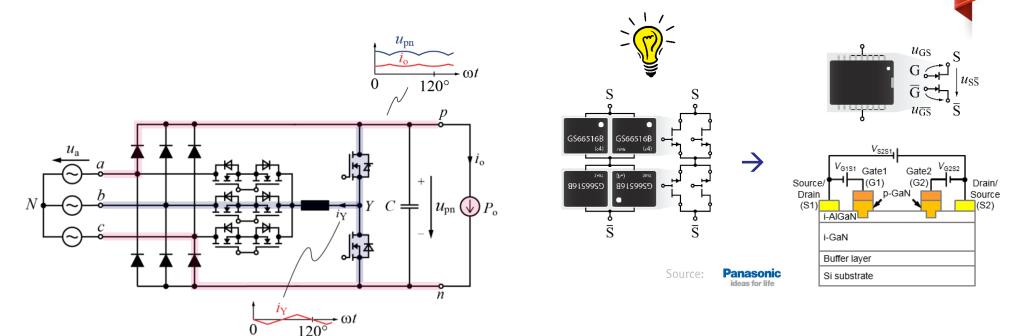






Remark Application of M-BDSs (1)

- M-BDS Monolithic Bidirectional / Bipolar Switch Realization of the Phase Selector Switches of 3rd Harmonic Inj. PFC Rectifiers Bipolar Voltage Blocking / Current Carrying Capability



• M-BDS \rightarrow Factor of 4 Reduction of Chip Area Comp. to Discrete Realization of Same $R_{(on)}$ (!)

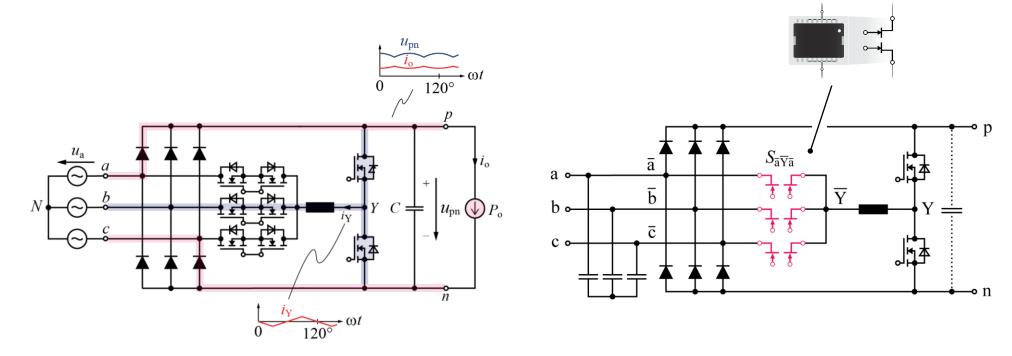






Remark Application of M-BDSs (2)

- Realization of the Phase Selector Switches of 3rd Harmonic Inj. PFC Rectifiers
 Bipolar Voltage Blocking / Current Carrying Capability
 Low Sw. Frequ. / Mains Frequ. Operation



• M-BDS \rightarrow Factor of 4 Reduction of Chip Area Comp. to Discrete Realization of Same $R_{(on)}$ (!)

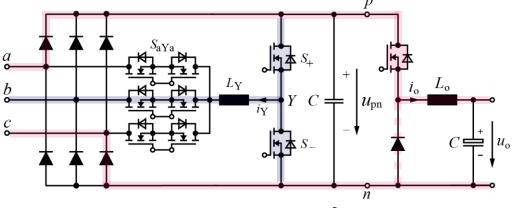


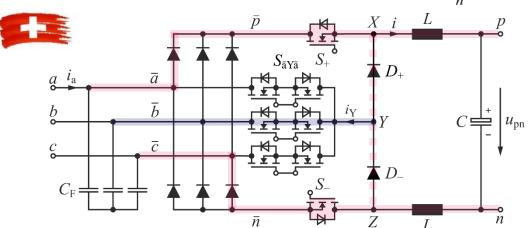


Swiss Rectifier

- Integration of 3rd Harmonic Injector Switches & Buck Output Stage Controlled Output Voltage Sinusoidal Mains Current

- \bullet i_y Def. by KCL: E.g. i_a i_c





• Low Complexity

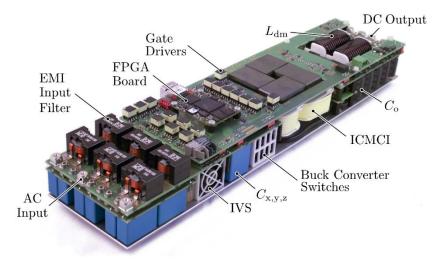




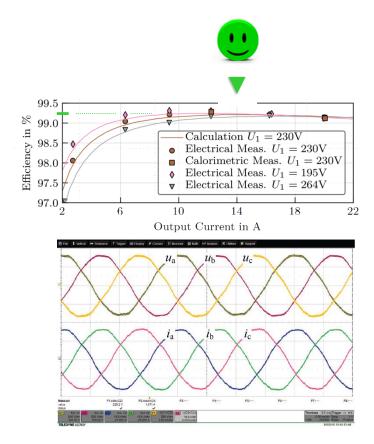
Swiss Rectifier Demonstrator

- Efficiency η = 99.26% @ 60% Rated Load Mains Current THD_I \approx 0.5% @ Rated Load Power Density $\rho \approx 4 \text{kW/dm}^3$

$$P_0$$
= 8 kW
 U_N = 400V_{AC} \Rightarrow U_0 = 400V_{DC}
 f_S = 27kHz

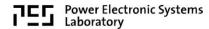


- SiC Power MOSFETs & Diodes
- Integr. CM & Output Coupling Inductors (ICMCI)





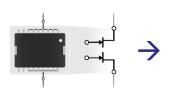


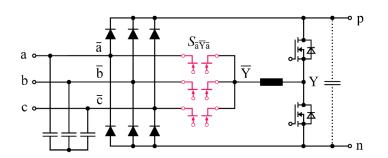


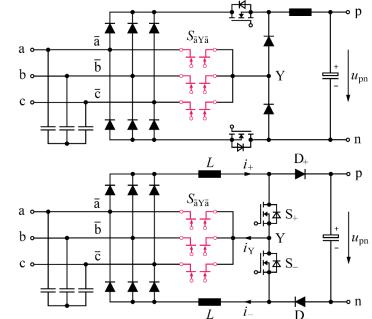


Remark M-BDS-Based 3rd Harm. Inj. Rectifiers

- Bipolar Voltage Blocking / Current Carrying Capability
 Factor of 4 Reduction of Chip Area Comp. to Discrete Realization of Same R_(on)







Mains Frequ. Operation of the Phase Selector Switches \rightarrow Conduction Losses Only

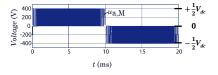






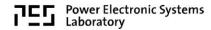


3-Level T-Type Boost PFC Rectifier



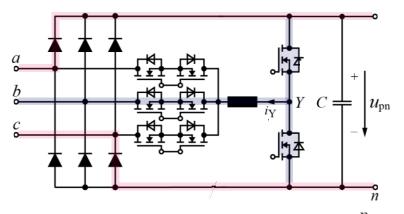






3-Level T-Type PFC (Vienna) Rectifier

- 3rd Harm. Inj. Inductor Shifted to AC-Side & PWM of DC-Midpoint Ref. Inj. Switches
- 3-Level Diode Bridge Input Voltage
- Sinusoidal Input Current
- Controlled Output Voltage





- Low Sw. Voltage Stress
- Low AC-Side Inductance
- Low Conduction Losses
- Bridge-Leg & Phase Symmetry



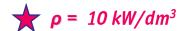


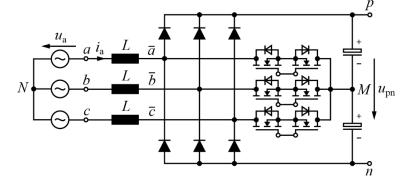
Vienna Rectifier Demonstrator (1)

- Design for More Electric Aircraft Application
 650V CoolMOS & 1200V SiC Diodes
- Coldplate Cooling

$$P_0$$
= 10 kW
 U_N = 400V_{AC}±10%
 f_N = 50Hz or 360...800Hz
 U_0 = 800V_{DC}

$$\eta = 96.8\%$$



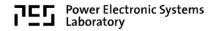




• $THD_i = 1.6\%$ @ $f_N = 800$ Hz ($f_P = 250$ kHz)





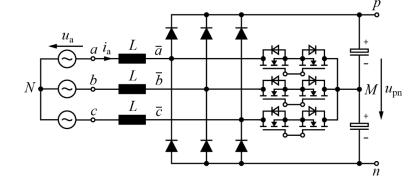


Vienna Rectifier Demonstrator (2)

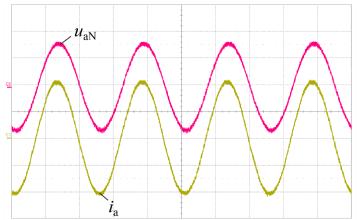
- Design for More Electric Aircraft Application
 650V CoolMOS & 1200V SiC Diodes
- **■** Coldplate Cooling

$$P_0$$
= 10 kW
 U_N = 400V_{AC}±10%
 f_N = 50Hz or 360...800Hz
 U_0 = 800V_{DC}

$$\eta = 96.8\%$$
 $\rho = 165 \text{ W/in}^3 (10 \text{ kW/dm}^3)$
 $f_P = 250 \text{kHz}$







- THD_i = 1.6% @ f_N = 800Hz
 System Allows 2-Φ Operation

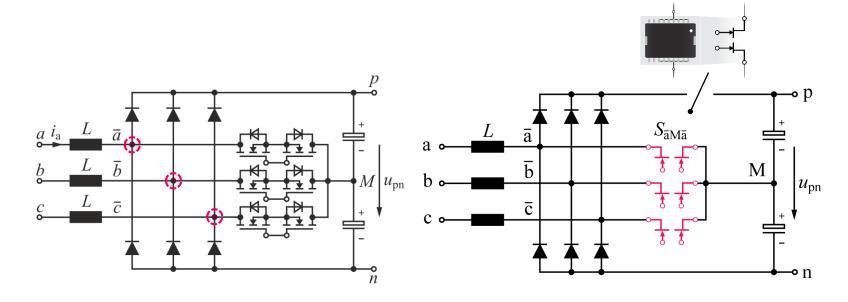






Remark Application of M-BDSs

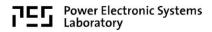
- M-BDS-Realization of the Midpoint-Switches
- Significant Reduction of Cond. Losses @ Given Chip Area



• 600 V M-BDSs @ U_{pn} = 800 V_{DC} in Combination w/ 1200 V SiC Diodes (MOSFETs for Bidir. Power Flow)









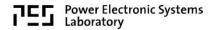
Global Megatrends



Digitalization
Renewable Energy
Sustainable Mobility
Industry Automation
Etc.





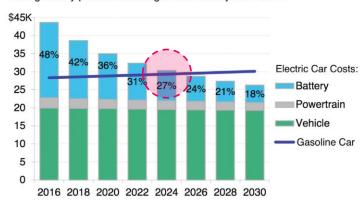


Electric Vehicle Outlook 2019

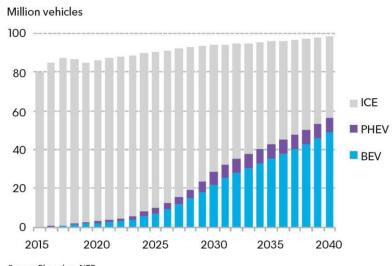
■ Bloomberg NEF — By 2040 — 57% of All Passenger Vehicle Sales 30% of Global Passenger Vehicle Fleet

Electric Cars Will Win on Price

Falling battery prices undercut gasoline cars by mid-2020s



Global long-term passenger vehicle sales by drivetrain



Source: BloombergNEF

• Falling Battery Costs → Price Parity of EVs & ICE-V by Mid-2020s → Tipping Point for EV Industry





Disruptive Innovations

- Example Rapid Change of Transportation Enabled by New Technology (ICE) & Business Model Tony Seba: "All New Vehicles, Globally, will be Electric by 2030"
- NY City, 5^{th} Av., Easter Parade → Year 1900: One Motor Cycle / Year 1913: One Horse & Carriage (!)



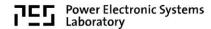


Source: Tony Seba

- Further Examples Digital / Analogue Photography, VHS Cassette Tape System / DVD etc.
 The Stone Age Didn't End for the Lack of Stone (Disrupted by Bronze Tools)







Ultra-Fast/High-Power EV Charging

- Modular Mains Interfaces | Future Non-Isolated Virtually Grounded Systems
 Very Wide Output Voltage Range (200...800V)



ChargePoint stations (projected growth)

2019 2025



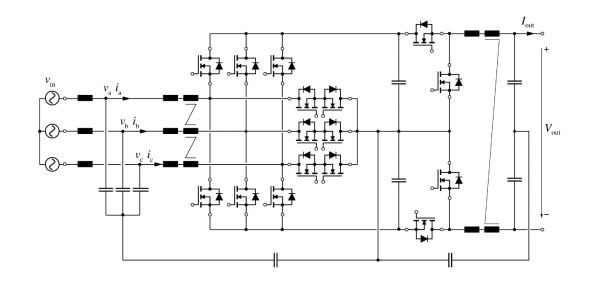
- Local Battery Buffer
- 320kW → 500km Range in 20min

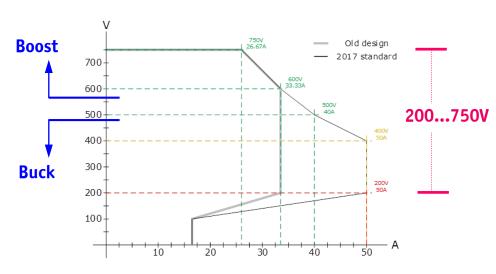




Bidirectional *Boost-Buck* PFC Rectifier Concepts

- Vienna Rectifier Type Bidirectional Boost PFC AC/DC Front-End & DC/DC Buck Output Stage Coordinated "Synergetic Control" of AC/DC and DC/DC Converter Stage for Min. Sw. Losses

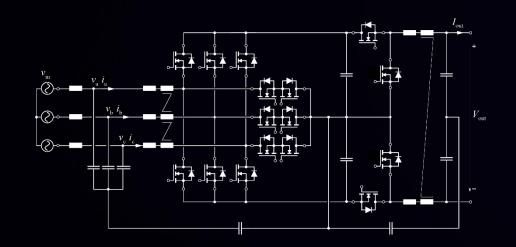




Future Non-Isolated EV-Charging → Earth Leakage Curr. Limited Using "Virtual Ground Control"





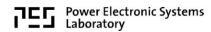




Boost-Buck

DUA ITY

Buck-Boost



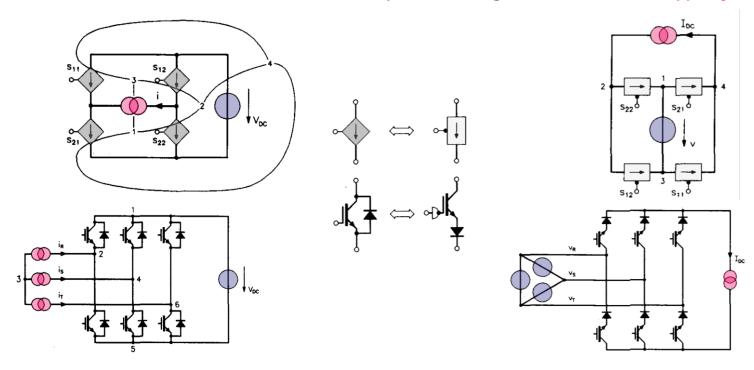


IEEE TRANSACTIONS ON INDUSTRY APPLICATIONS, VOL. 29, NO. 2, MARCH/APRIL 1993

Quasi-Dual Modulation of Three-Phase PWM Converters

Johann W. Kolar, Member, IEEE, Hans Ertl, Member, IEEE, and Franz Zach, Member, IEEE

- Duality of Voltage DC-Link & Current DC-Link Converter Circuits
 Unipolar Blocking / Bidir. Current \rightarrow Bipolar Blocking Unidir. Switches \rightarrow Appl. of M-BDSs (!)



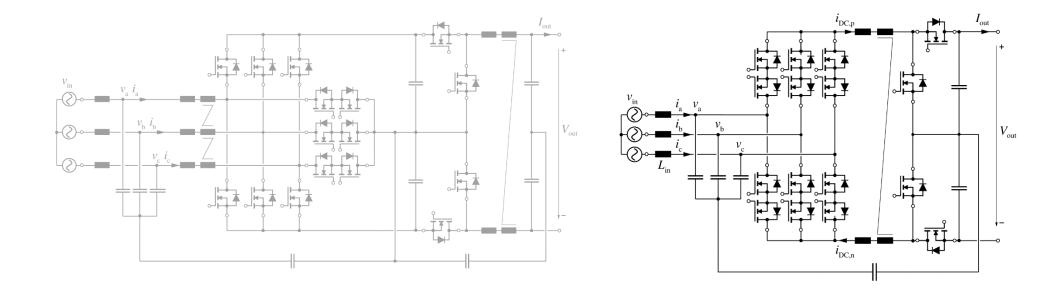






Bidirectional Buck-Boost PFC Rectifier Concepts

- Boost—Buck OR Buck—Boost Combination
- Closed Loop vs. Open Loop Mains Current Control & Active Input Filter Damping
 "Synergetic Control" of AC/DC and DC/DC Converter Stage



AC/DC Buck-Stage Output Inductor Utilized as DC/DC Boost Inductor \rightarrow Min. # of Inductive Components





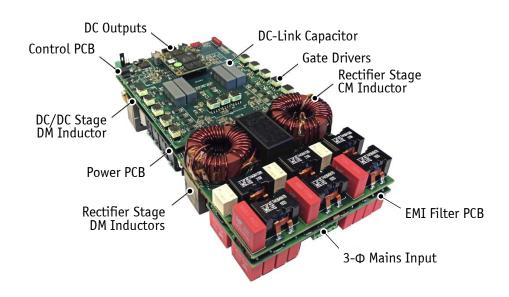
Boost-Buck | **Buck-Boost** Demonstrator Systems

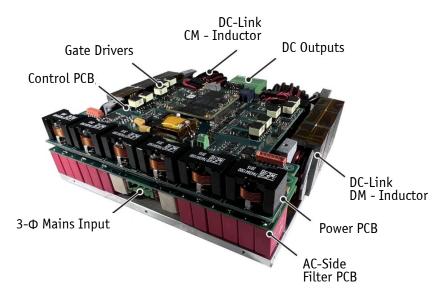
- 10 kW @ 400...800 V_{DC} @ 3- Φ 400 V_{rms} Mains $U_{out} = 200 \dots 800 V_{DC}$ $\eta = 98.8\%$ @ 5.4 kW/dm³

- $AC/DC f_{sw} = 100 \text{ kHz}$ $DC/DC f_{sw} = 2 \times 100 \text{ kHz} / 200 \text{ kHz}$ eff.

- $10 \text{ kW} @ 400...1000 \text{ V}_{DC} @ 3-\Phi 400 \text{ V}_{rms} \text{ Mains}$ $U_{out} = 200 ... 1000 \text{ V}_{DC}$ $\eta = 98.6\% @ 6.4 \text{ kW/dm}^3$

- $AC/DC f_{sw} = 100 \text{ kHz}$ $DC/DC f_{sw} = 2 \times 50 \text{ kHz} / 100 \text{ kHz}$ eff.





- **Boost-Buck** Voltage DC-Link PFC Rectifier
- **Buck-Boost** Current DC-Link PFC Rectifier

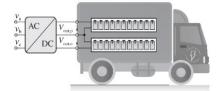


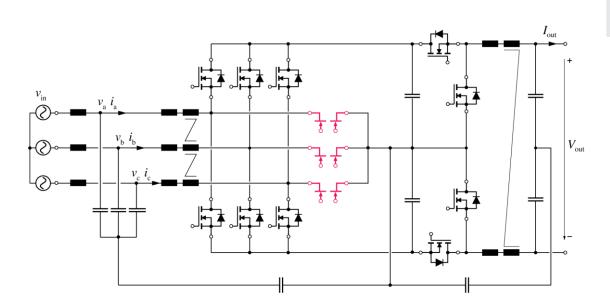


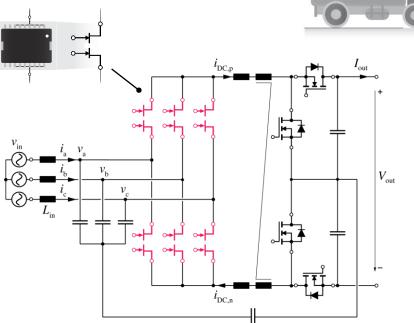


Remark Application of M-BDSs

- Boost—Buck OR Buck—Boost Combination
- Closed Loop vs. Open Loop Mains Current Control & Active Input Filter Damping
- "Synergetic Control" of AC/DC and DC/DC Converter Stage



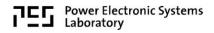




600 V M-BDSs for Boost—Buck & 1200 V M-BDSs for Buck—Boost Combination @ 400 V_{rms} Mains









3-Ф Isolated Matrix-Type Single-Stage — PFC Rectifier

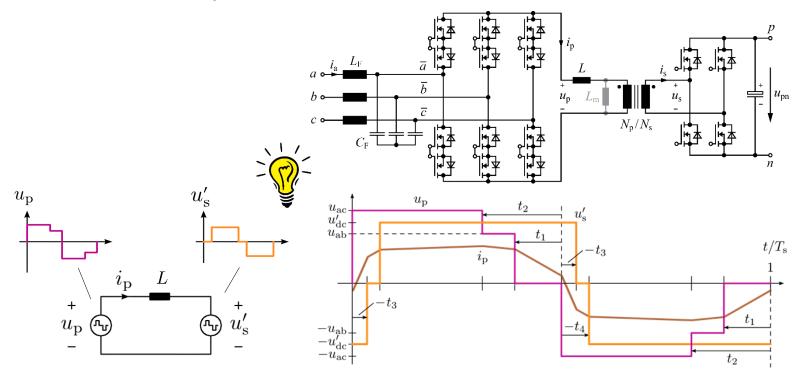






Isolated Matrix-Type PFC Rectifier (1)

- Based on Dual Active Bridge (DAB) Concept Opt. Modulation $(t_1...t_4)$ for Min. Transformer RMS Curr. & ZVS or ZCS Allows Buck-Boost Operation

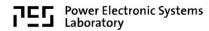


• Equivalent Circuit

• Transformer Voltages / Currents



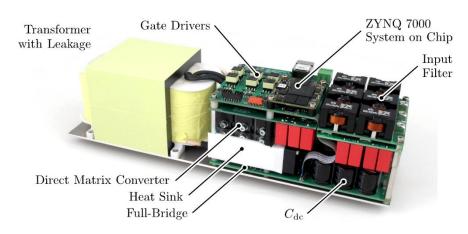




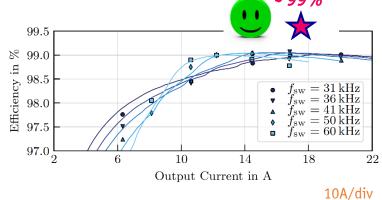
Isolated Matrix-Type PFC Rectifier (2)

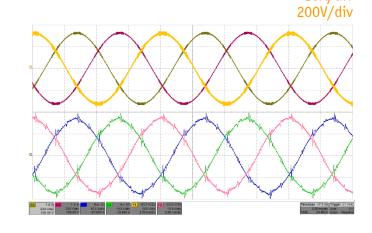
- Efficiency η = 98.9% @ 60% Rated Load (ZVS) Mains Current THD_I ≈ 4% @ Rated Load Power Density ρ ≈ 4kW/dm³

$$P_0$$
= 8 kW
 U_N = 400V_{AC} $\rightarrow U_0$ = 400V_{DC}
 f_S = 36kHz



- 900V / 10mΩ SiC Power MOSFETs
 Opt. Modulation Based on 3D Look-Up Table





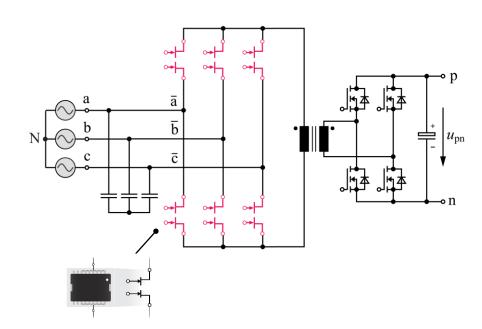


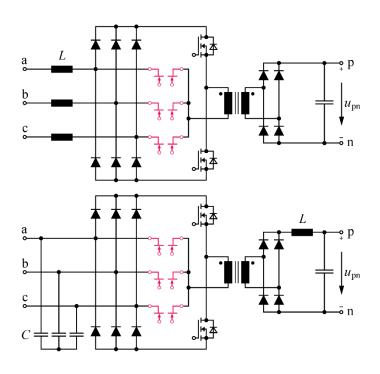




Remark Application of M-BDSs

- Matrix-Type Bidirectional DAB-Based Topology Unidir. Vienna Rectifier II (Boost-Type) Unidir. Vienna Rectifier III (Buck-Type)

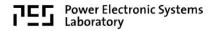




• Functional Integration → Lower Complexity BUT Limited Controllability



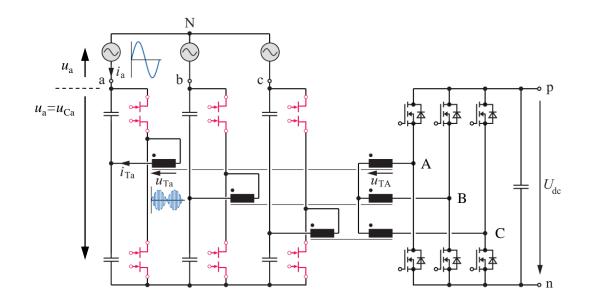


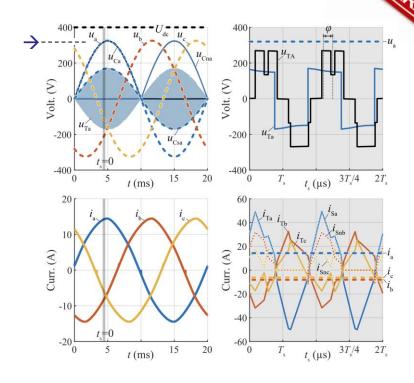




Remark Phase-Modular Isolated Matrix-Type PFC Rectifier

- **Voltage Stress on AC-Side Power Transistors Determined by PHASE Voltage Amplitude (!)**
- 600V GaN MBDS for 400V RMS Line-to-Line Grid (U_{pk} = 560V) Unity Power Factor / Bidirectional

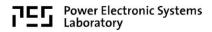




- Dual Active Bridge-Type Control
- AC-Side Phase Modularity Full Rated Power Operation @ 1-Ф Input (!)









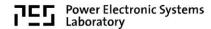




Digitalization Sustainable Mobility Renewable Energy Industry Automation — Etc.







<u>Variable Speed Motor Drive (VSD) Systems</u>

- Industry Automation / Robotics
 Material Machining / Processing Drilling, Milling, etc.
- Compressors / Pumps / FansTransportation
- etc., etc.

.... Everywhere!

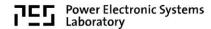




• 60...70 % of All Electric Energy Used in Industry Consumed by VSDs

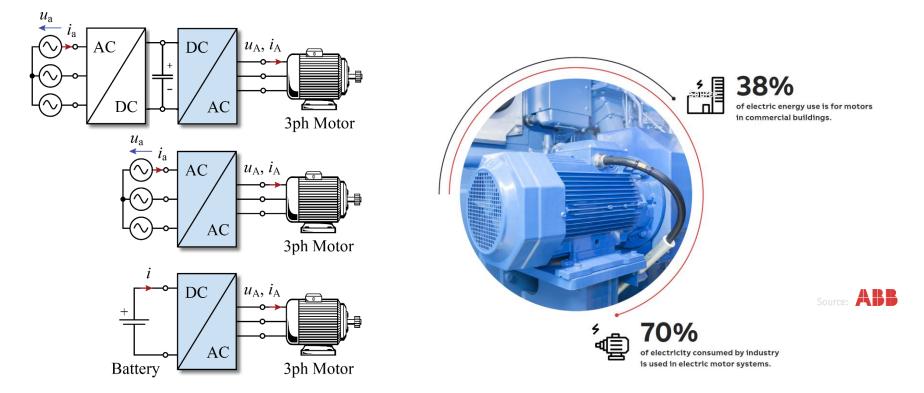






Variable Speed Drive Concepts

- DC-Link Based AC/DC/AC OR Matrix-Type AC/AC Converters Battery OR Fuel-Cell Supply OR Common DC-Bus Concepts



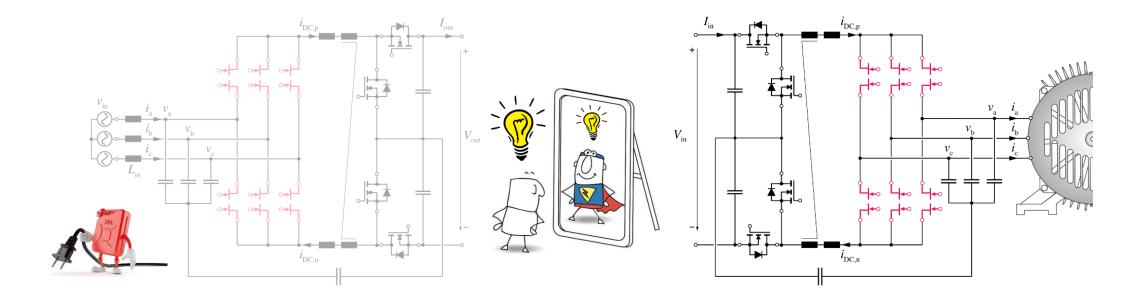
• 45% of World's Electricity Used for Motors in Buildings & Industrial Applications





Current DC-Link Buck-Boost Inverter (1)

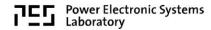
- Derivation Based on Bidirectional Buck-Boost PFC Rectifier Topology (EV Charger) Lower # of Ind. Components Compared to Boost-Buck Approach



- DC/DC Buck Converter Performs Voltage → Current Translation Coordinated Control / Modulation of DC/DC & Inverter Stage for Min. Sw. Losses

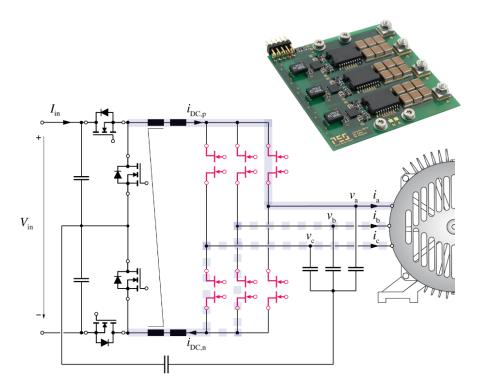


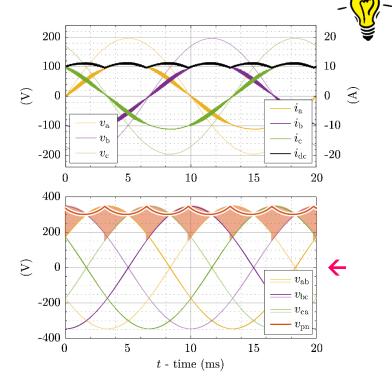




Current DC-Link Buck-Boost Inverter (2)

"Synergetic" Control of DC/DC Buck Converter & Current DC-Link Inverter Stage 6-Pulse-Shaping of DC Current by Buck-Stage → Allows Inverter Phase Clamping

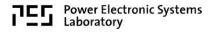




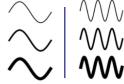
Switching of Only 2 of 3 Phase Legs \rightarrow Reduction of Sw. Losses by \approx 86% (!)





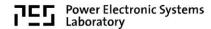






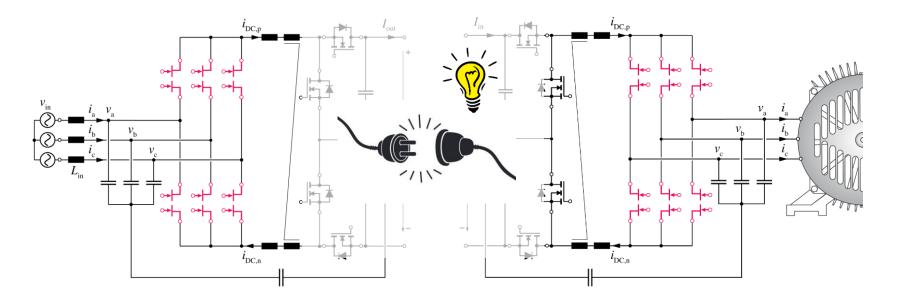






3-Φ Current DC-Link AC/AC Converter (1)

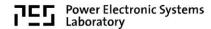
- DC-Side Coupling of Buck-Boost Current DC-Link PFC Rectifier & Inverter AC/DC/AC
- Full Sinewave Filtering @ Input & Output w/ Single Magnetic Component



- Bipolar Blocking / Unidir. Switches / Unidir. DC-Link Current Sufficient for Bidir. Power Conversion
- ullet Modulation-Based Inversion of DC-Link Voltage Polarity ullet Inv. of Power Flow Direction

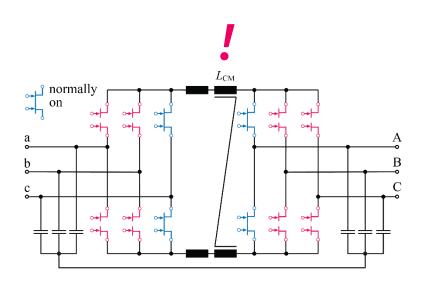


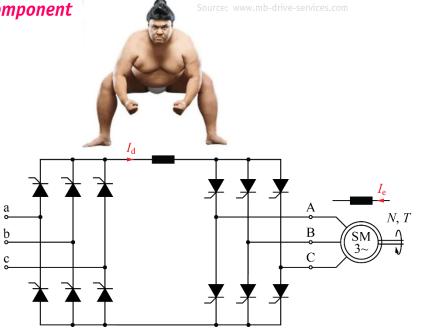




3-Φ Current DC-Link AC/AC Converter (2)

Sinusoidal Motor Voltage Achieved w/ Single Ind. Component Unidir. Valves Sufficient for Bidir. Power Conversion M-BDSs — Synchronous Rectification

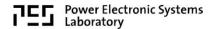




• Relation to High-Power Thyristor-Based Medium Voltage Synchr. Machine Variable Speed Drives





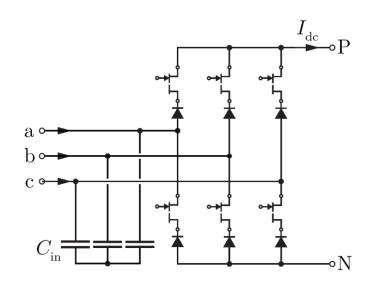


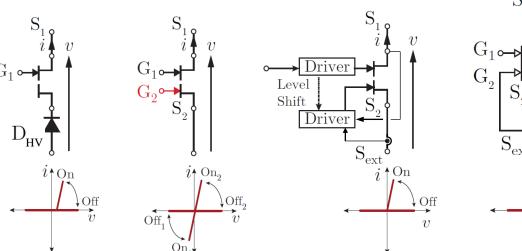


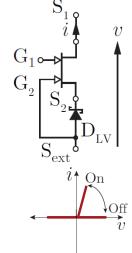
Remark Self Reverse-Blocking M-BDS-Concept (1)

- Bidir. Curr. DC-Link Converters Unidir. I_{dc} & Bipolar U_{dc} OR Bidir. I_{dc} & Unipolar U_{dc}
- HV Switch + HV Diode
- M-BDS
- "Self-Switching"

HV Diode Characteristic / High Cond. Losses Ohmic Cond. Char. BUT 2 External Gate Signals / 2 Gate Drives Ohmic Cond. Char. BUT High Local Complexity (Sensing)



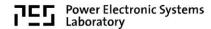




SRB-MBDS Quasi-Ohmic Cond. Char. (Cascode w/ LV Si Schottky Diode) & 1 External Gate







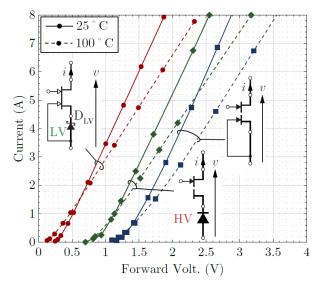


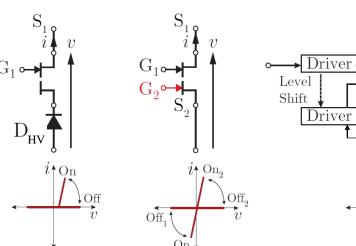
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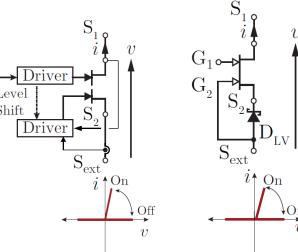
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- M-BDS
- "Self-Switching"

HV Diode Characteristic / High Cond. Losses Ohmic Cond. Char. BUT 2 External Gate Signals / 2 Gate Drives Ohmic Cond. Char. BUT High Local Complexity (Sensing)

 $600\,\text{V}$ 190 m Ω GaN M-BDS 40 V/10 A Si Schottky Diode







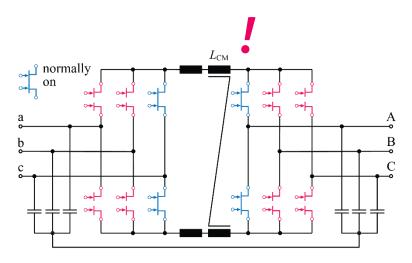
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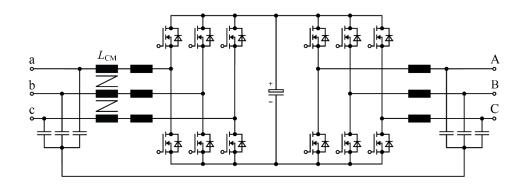




- Current DC-Link Topology
- Application of M-BDSs
- Complex 4-Step Commutation
- Low Filter Volume



- Voltage DC-Link Topology
- **Standard Bridge-Legs**
- Low-Complexity Commutation
 Defined Semiconductor Voltage Stress
- Facilitates DC-Link Energy Storage



- **Challenging Overvoltage Protection**
- **Limited Control Dynamics**

High Input / Output Filter Volume

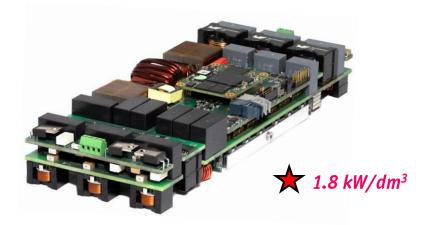




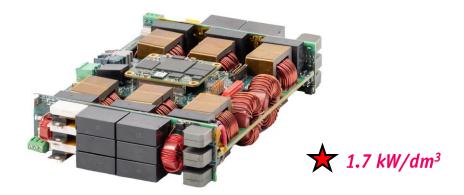




- Current DC-Link Topology
- Application of M-BDSs
- Complex 4-Step Commutation Low Filter Volume



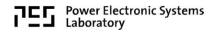
- Voltage DC-Link Topology
- **Standard Bridge-Legs**
- Low-Complexity Commutation
 Defined Semiconductor Voltage Stress
- Facilitates DC-Link Energy Storage



■ All-600V-GaN AC-AC VSDs / 1.4 kW, 200 V L-L / Full EMI Filter (Grid & Motor) / 97% Nominal Eff.









3-Φ AC/AC
Matrix Converter

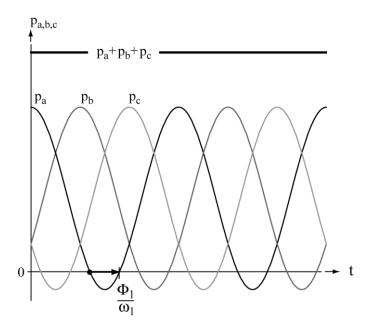
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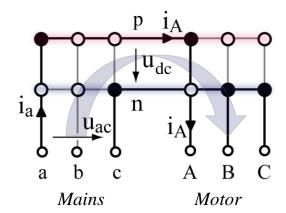


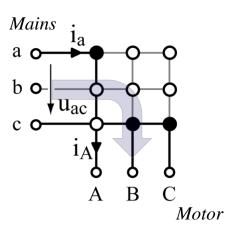


Indirect & *Direct* 3-Ф AC/AC Matrix Converter (1)

- Constant 3- \oplus Instantaneous Power Flow \rightarrow No Low-Frequ. DC-Link Power Pulsation Buffer Requirement (!)
- Indirect AC/DC—DC/AC OR Direct AC/AC Power Conversion → IMC OR DMC Switch Matrix w/ Bipolar Voltage Blocking & Current Carrying Devices







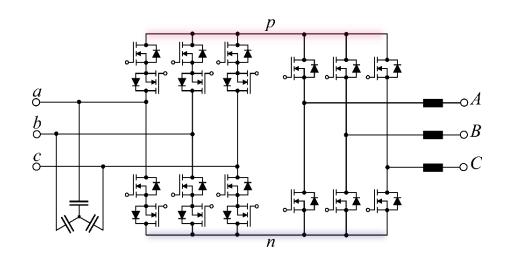
Output-Side Motor Inductor \rightarrow Operation Limited to Buck-Type (Step-Down) Voltage Conversion

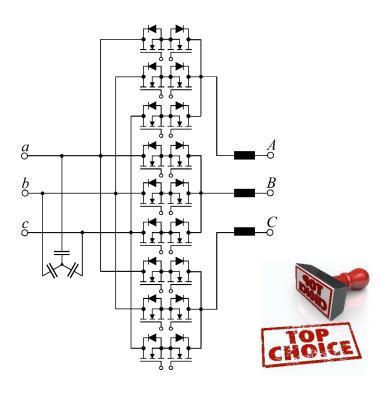




Indirect & *Direct* 3-Ф AC/AC Matrix Converter (2)

- Input Filter Capacitors | Sw. Stage | Motor Inductance Buck-Type Power Conversion Topology

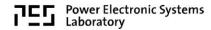




- IMC Relies on Strictly Pos. DC-Link Voltage / i=0 Input Stage Commutation
- M-BDS-Based Realization of DMC Features Lower # of Switches / 4-Step Commutation Required



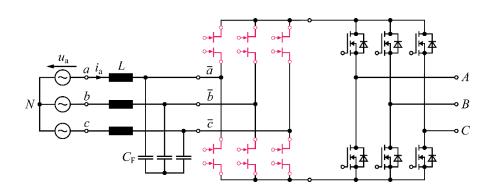




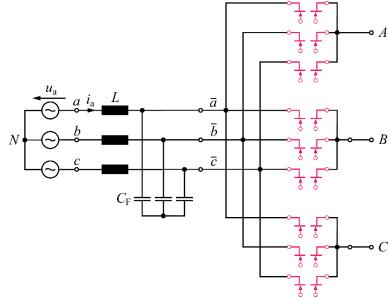


Remark Application of M-BDSs

- Indirect Matrix Converter (IMC)
- M-BDS AC/DC Front-End ZCS Commutation of AC/DC Stage @ i_{DC} =0 No 4-Step Commutation



- Direct Matrix Converter (DMC)
- 4-Step Commutation Exclusive Use of M-BDSs



- **Higher # of Switches Compared to DMC**
- Lower Cond. Losses @ Low Output Voltage Thermally Critical @ $f_{out} \rightarrow 0$

• Thermally Critical @ $f_{out} \approx f_{in}$







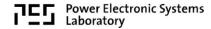


Selected GaN & SiC M-BDS R&D Activities



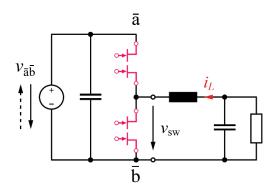


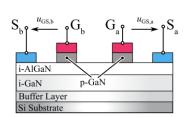


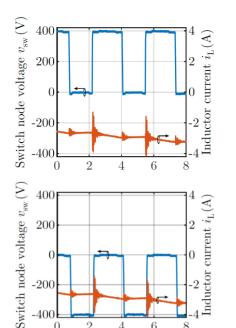


Experimental Analysis of 1st Gen. 600V GaN M-BDS

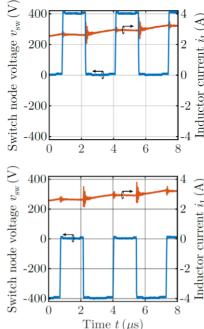
- POWERAMERICA Program Based on Infineon's CoolGaN™ HEMT Technology Dual-Gate Device / Controllability of Currents in Both Directions
- Bipolar Voltage Blocking Capability | Normally-On or Normally-Off







Time $t(\mu s)$

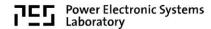




- Analysis of 4-Quardant Operation of $R_{DS(on)}$ = 140m Ω | 600V Sample @ ± 400V Shared Drift Region \rightarrow "True" Monolithic Bidirectional Switch (TM-BDS)

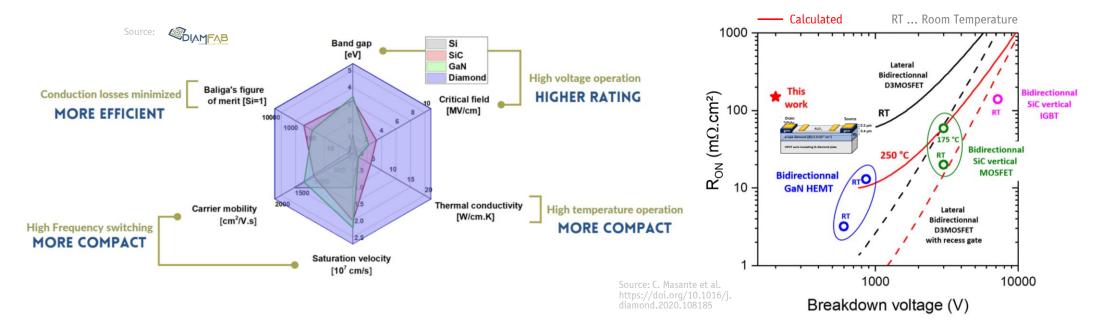






Monolithic Bidirectional Diamond Switch

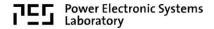
- Diamond High Breakdown Field / High Carrier Mobility / High Therm. Conductivity Lateral / Single Drift Layer Double-Gate Reverse Blocking & Reverse Conducting Power MOSFET



- Very Basic Proof of Concept @ 250°C
- Lateral Bidir. Diamond Devices Could Outperform Bidir. Vertical 4H-SiC Devices @ High Temp.

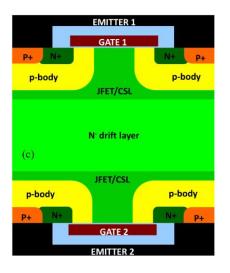


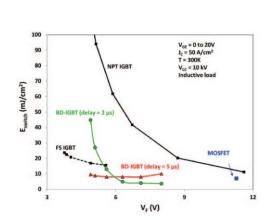


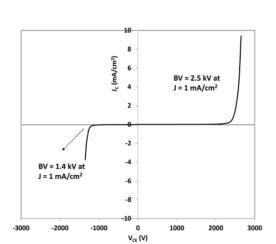


Monolithically Integrated Bi-Directional SiC IGBT

- Planar-Gate Bi-Direct. IGBT Fabricated w/ Double-Sided Lithography Process on Free-Standing n[—] Wafers
- MOS-Cells on Both Sides of Lightly Doped Drift Region / Cond. & Sw. Loss Infl. by Back-Side Gate Volt. Bias
- Challenging Packaging & Cooling



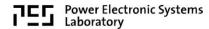




Chow et al., 2016

- Simul. Performance of a 15kV BD-IGBT | Blocking Characteristic (max. 7.2 kV Meas.) − Epi Layer Defects etc.
 Shared Drift Region → "True" Monolithic Bidirectional Switch (TM-BDS)

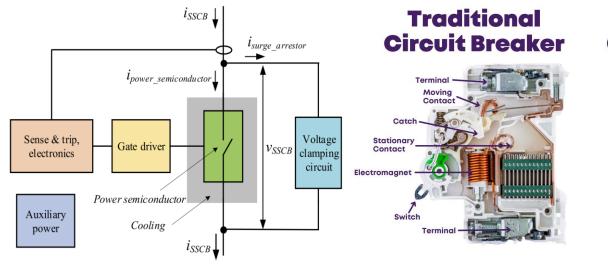






Remark Solid-State Circuit Breakers (SSCBs)

- Ultra-Fast Fault Interruption | Reduced Fault Stress | Arc-Less | Low Surge Voltage | Long Lifetime
- Software / Remote Configurable Trip Behavior / Remote-Controlled Load Switch



Solid-State Circuit Breaker

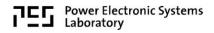


Rodrigues et al., 2021

- Recent LV Example w/ Custom SiC Modules / Max. 100A Cont. / UL-Certified M-BDSs Low On-Resistance Mandatory (e.g. 1100V, $22m\Omega$ GaN M-BDS) | Low Leakage Current





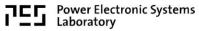




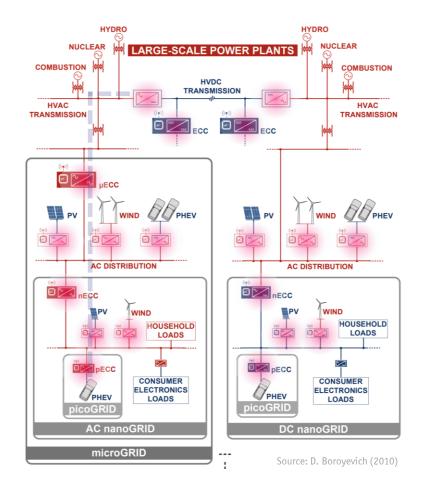








The in the Room



- **25'000 GW** Installed Ren. Generation in 2050
- 15'000 GWh Batt. Storage
- 4x Power Electr. Conversion btw Generation & Load
- 100′000 GW of Installed Converter Power
- 20 Years of Useful Life



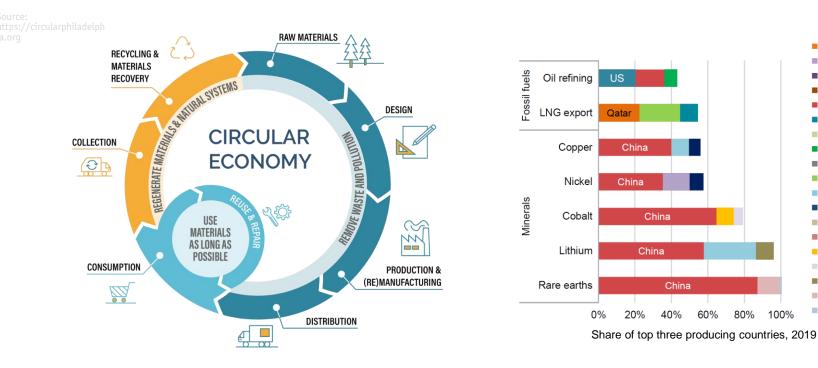
- 5'000 GW_{eq} = 5'000'000'000 kW_{eq} of E-Waste / Year (!) 10'000'000'000 \$ of Potential Value





The Paradigm Shift

- "Linear" Economy / Take-Make-Dispose → "Circular" Economy / Perpetual Flow of Resources Resources Returned into the Product Cycle at the End of Use



Qatar

DRC

US

Russia

■ Iran Australia

Chile

■ Japan

■ Peru

Finland

■ Belgium

■ Argentina

■ Malaysia Estonia

100%

■ Myanmar

Indonesia

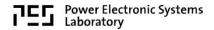
■ Philippines China

Saudi Arabia

■ Geographically Concentrated Production of Many Energy Transition Critical Minerals







Power Electronics 5.0

- Power Electronics 1.0 \rightarrow Power Electronics 5.0
- X-Technologies & X-Concepts

